



# Pellet core fueling in tokamaks, stellerators and reversed field pinches

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Eleonore Geulin, Bernard Pégourié. Pellet core fueling in tokamaks, stellerators and reversed field pinches. AAPPS DPP 2022 - 6th Asia-Pacific Conference on Plasma Physics, Oct 2022, Online conference (Tokyo), Japan. cea-03949385

**HAL Id: cea-03949385**

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Submitted on 20 Jan 2023

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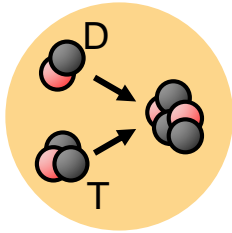
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# Pellet core fueling in tokamaks, stellerators and reversed field pinches

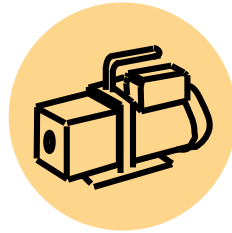
Eleonore Geulin, Bernard Pégourié

10/11/2022 - AAPPS conference

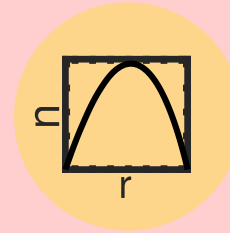
We need to fuel to compensate :



Fusion reactions



Ash pumping



Keep core  
density  
→ balancing  
outgoing flows

## Gaz puff injection



easy to use



Fuel only the edge of the plasma

→ Screening of neutrals in the SOL

## Neutral beam injection



Deep penetration



- Power & Matter injection

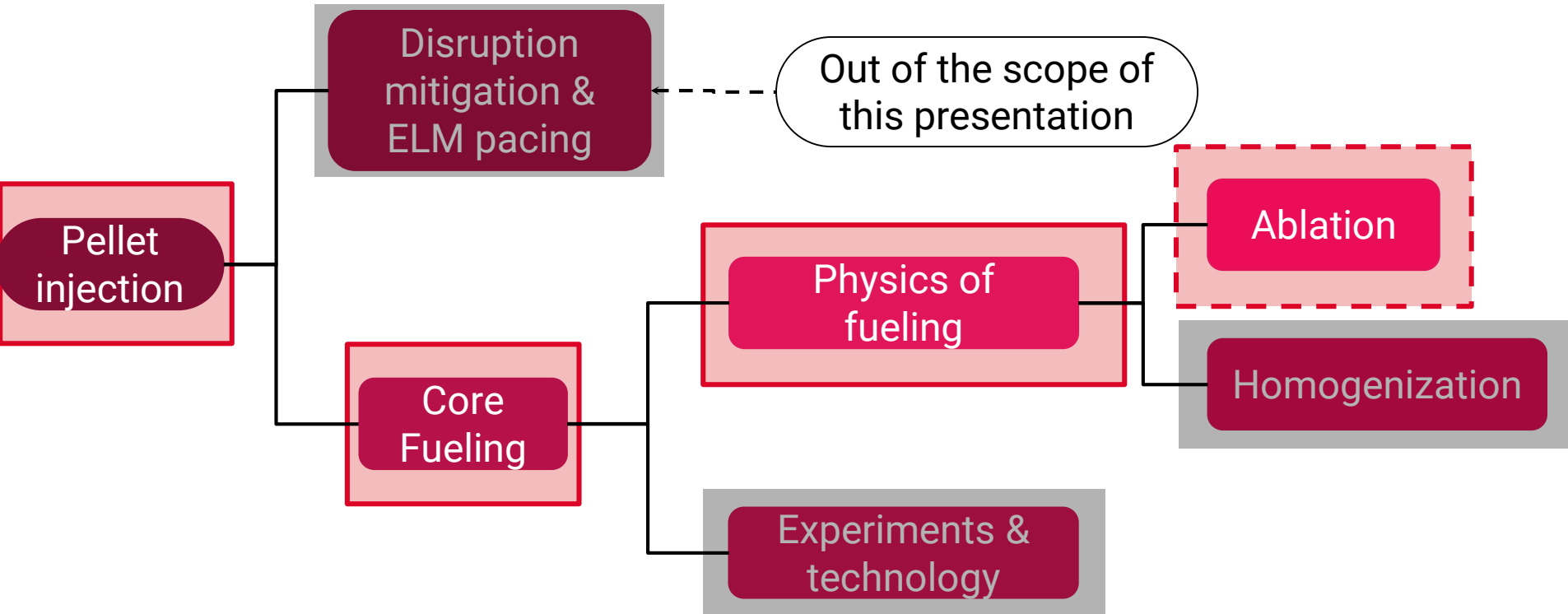
- Not enough fueling for required power

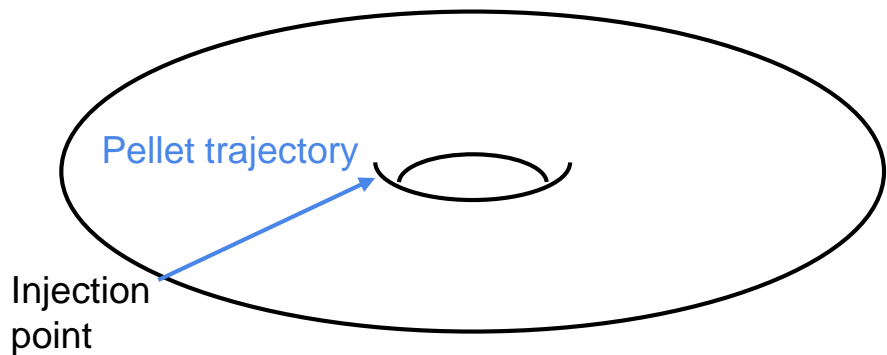
## Pellet injection

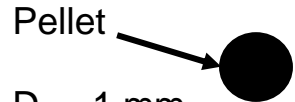
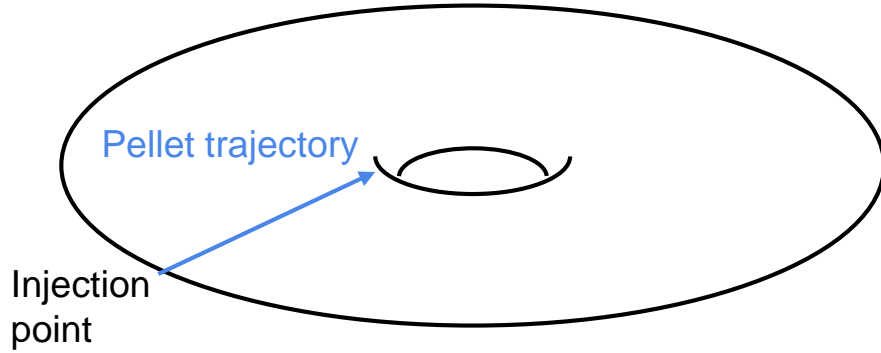


Deep penetration

Efficient fuelling with no momentum or power injection



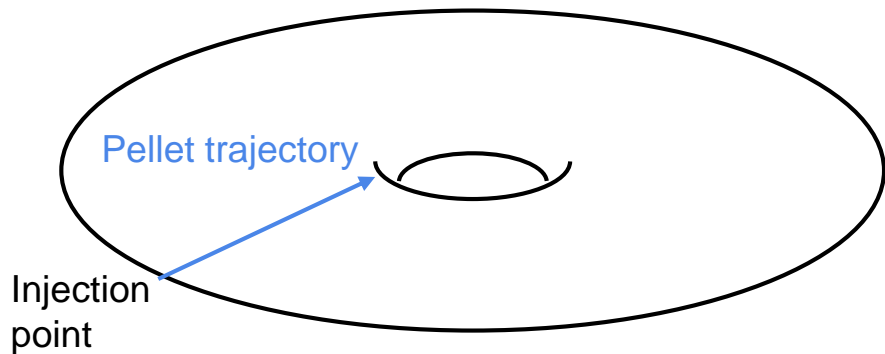




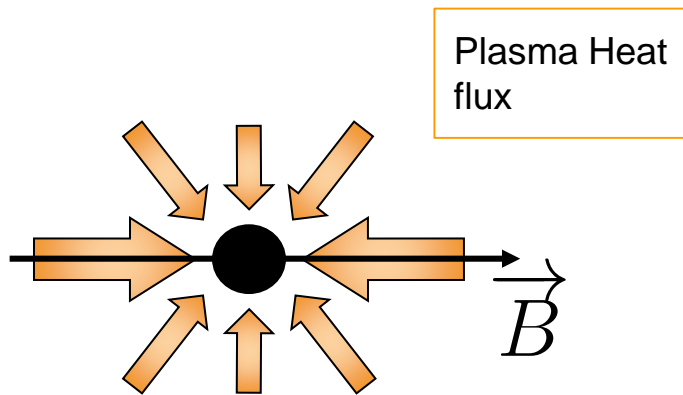
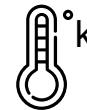
$D \sim 1 \text{ mm}$

$T^\circ \sim 15\text{K}$

$V \sim 200 \text{ m/s to a few km/s}$



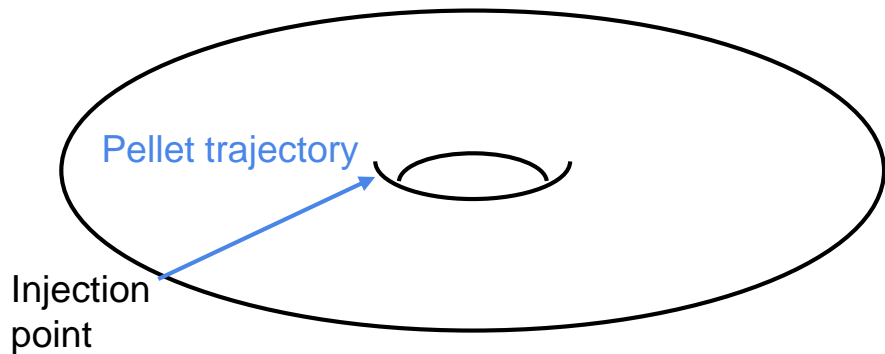
- By heating the pellet,



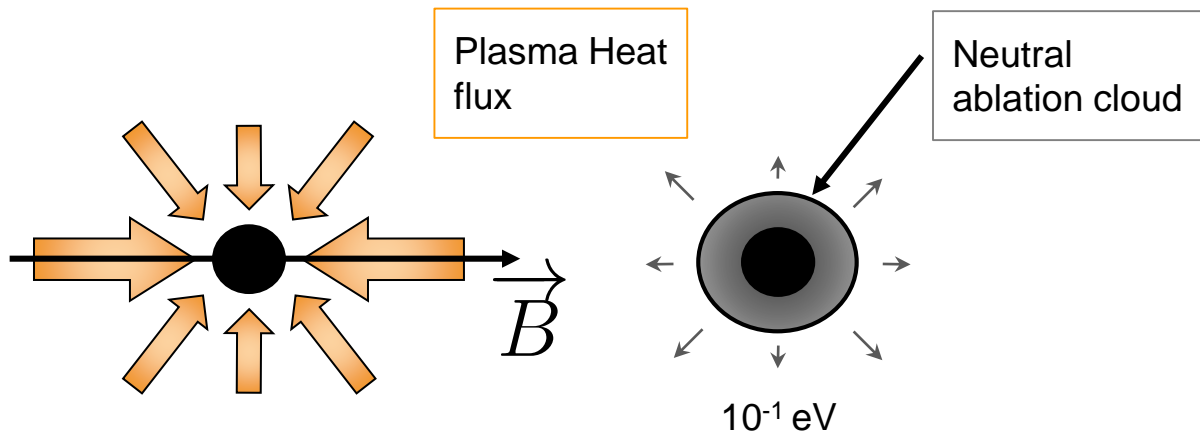
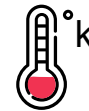
ablation : Loss of a material caused by vaporization



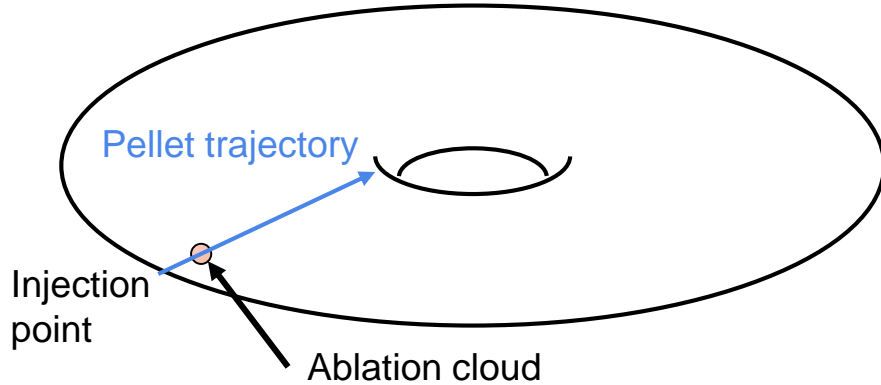
# Physic of ablation - Time story of a pellet immersed in plasma



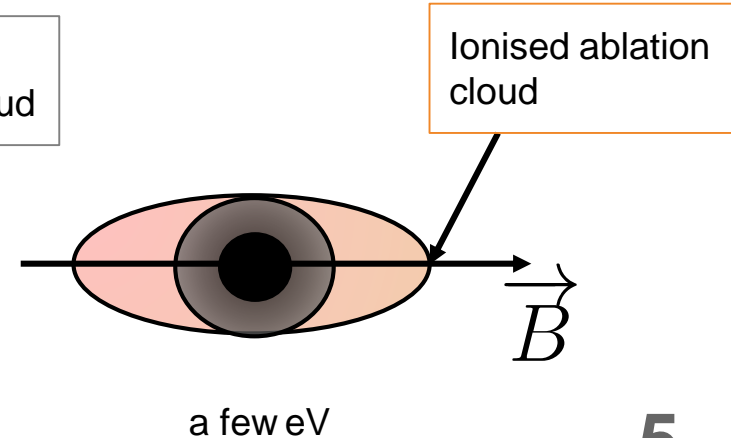
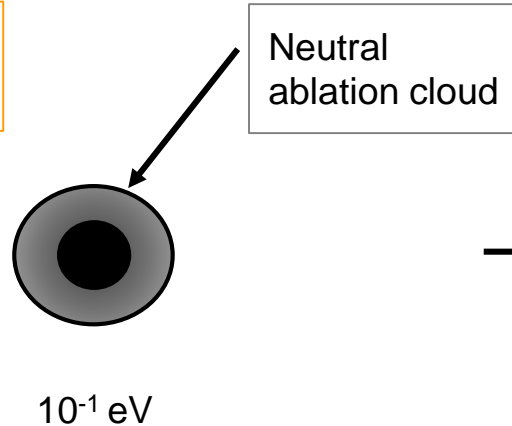
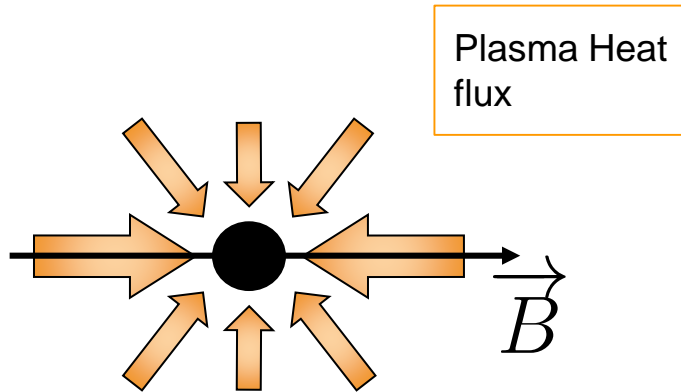
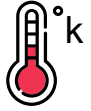
- By heating the pellet,  
⇒ Neutral ablation cloud



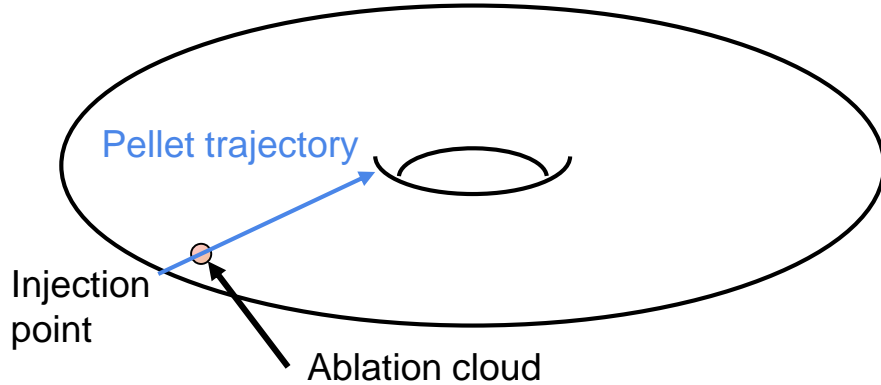
# Physic of ablation - Time story of a pellet immersed in plasma



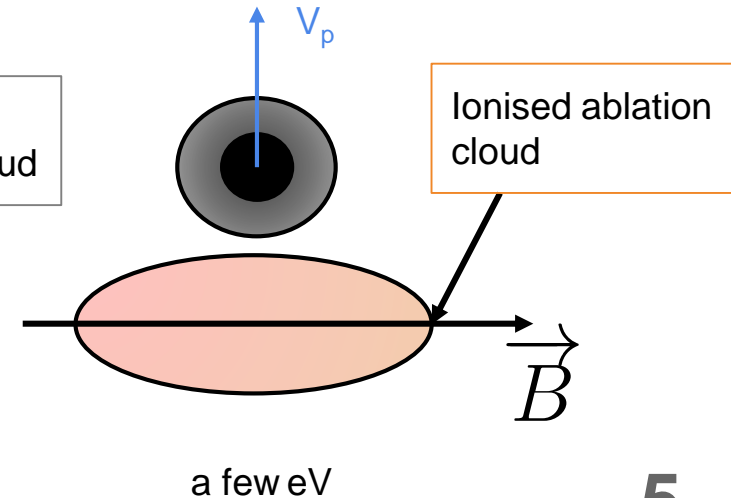
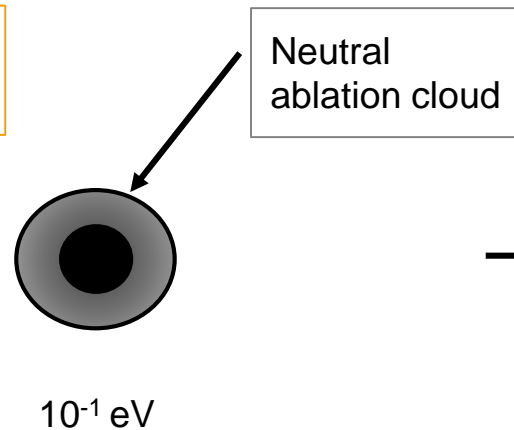
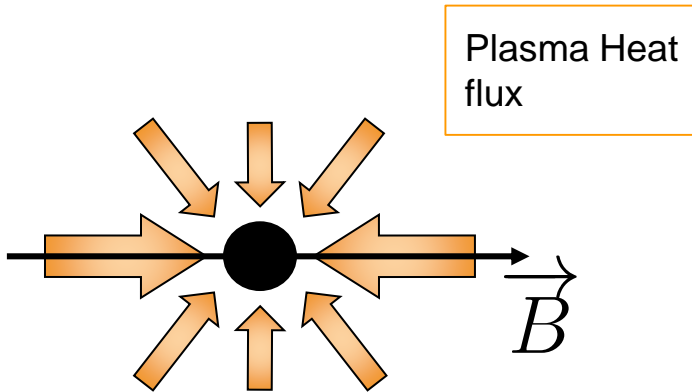
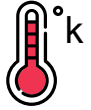
- By heating the pellet,  
 ⇒ Neutral ablation cloud  
 ⇒ Ionized ablation cloud



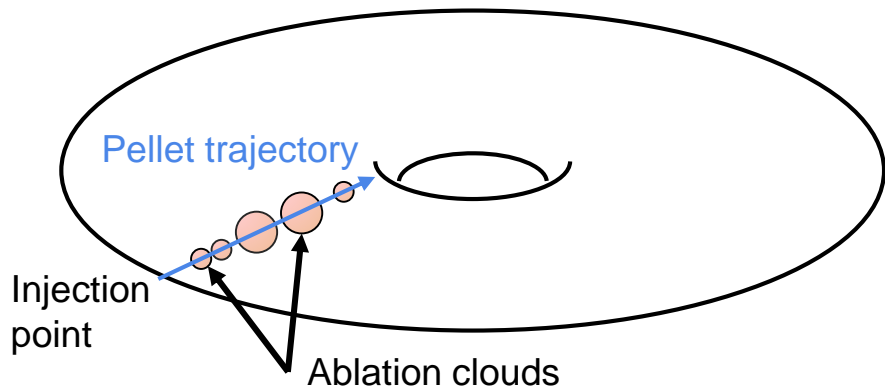
# Physic of ablation - Time story of a pellet immersed in plasma



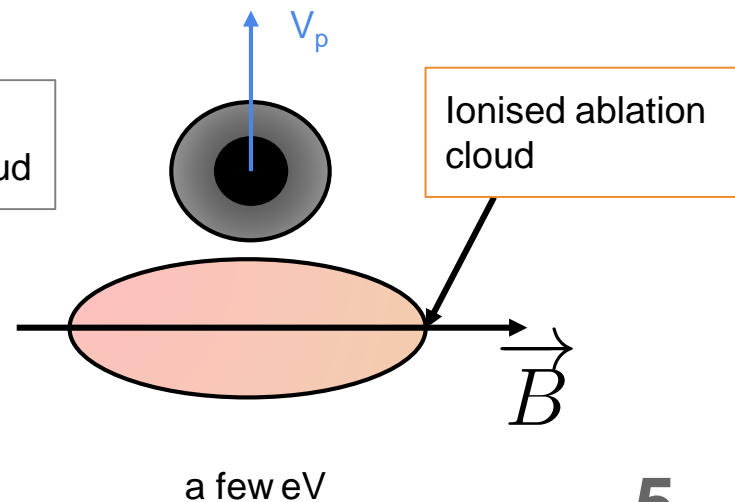
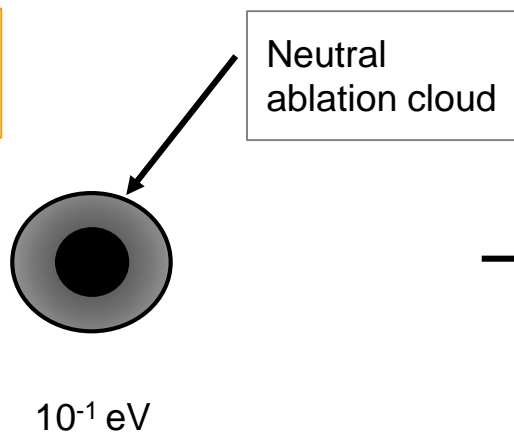
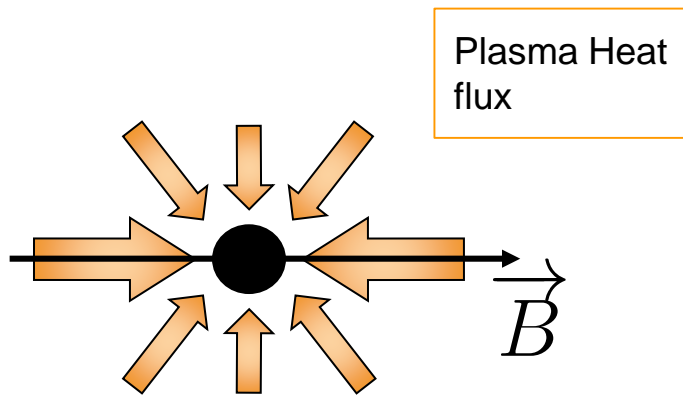
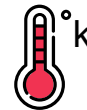
- By heating the pellet,  
 ⇒ Neutral ablation cloud  
 ⇒ Ionised ablation cloud
- Ionised ablation cloud separate from neutral part  
 (cloud + pellet).



# Physic of ablation - Time story of a pellet immersed in plasma



- By heating the pellet,  
 ⇒ Neutral ablation cloud  
 ⇒ Ionised ablation cloud
- Ionised ablation cloud separate from neutral part (cloud + pellet),  
 ⇒ Happens all along the pellet path



## Pellet penetration length :

$$L_p \propto V_{\text{pellet}} N_{\text{pellet}}^{1/2} n_{\text{plasma}}^{-1/3} T_{\text{plasma}}^{-5/3}$$

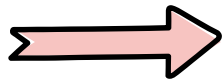
Diagram annotations: Red arrows point from the text "Pellet velocity / particle contents" to  $V_{\text{pellet}}$  and  $N_{\text{pellet}}$ . Another red arrow points from the text "Plasma density / temperature" to  $n_{\text{plasma}}$  and  $T_{\text{plasma}}$ . The exponents  $1/2$  and  $-5/3$  are circled in red.

Pellet velocity / particle contents

### 2 conclusions :

⇒ Temperature dependance is the more limiting for penetration

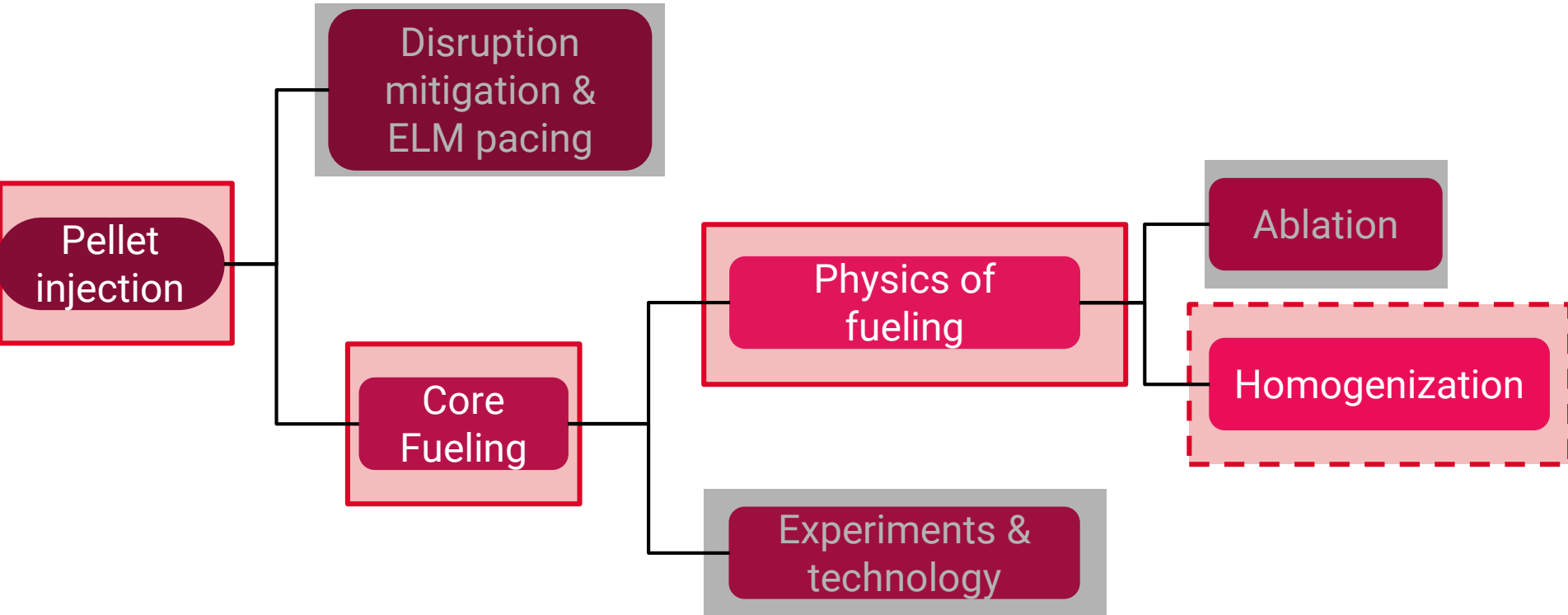
⇒ Increase  $V_p$  more efficient than  $N_p$  to increase  $L_p$



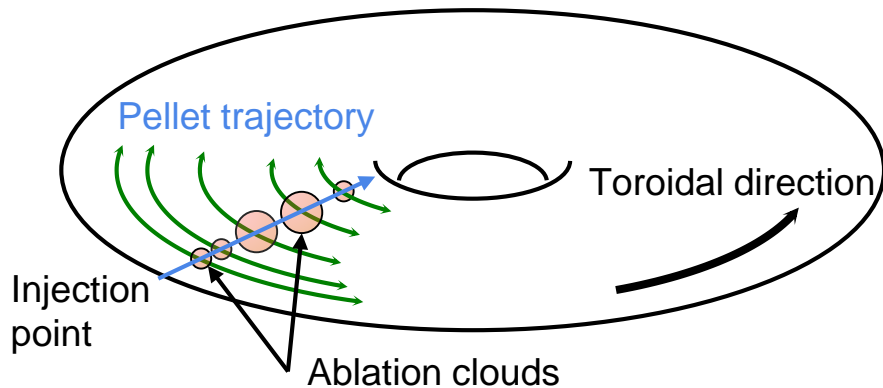
**Pellet  $L_p$  : from 20% to >50% plasma radius in present day tokamaks**

Fast ions (ICRH, NBI) moderate ablation increase

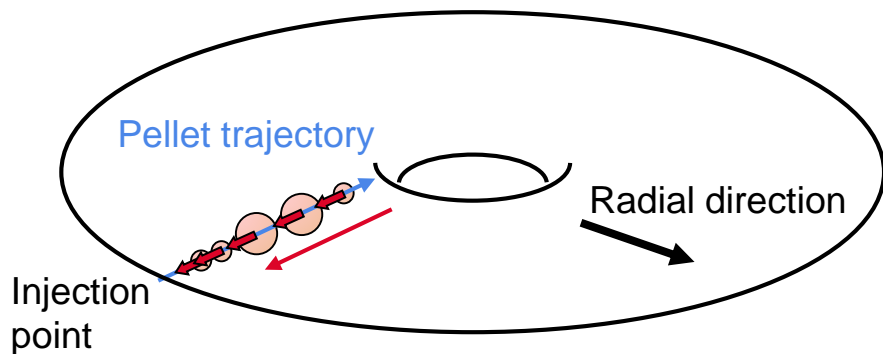
Fast electrons (ECRH) significant ablation increase; (LHCD) pellet mass sublimation



# During homogenization phase deposited matter moves on the parallel and radial direction



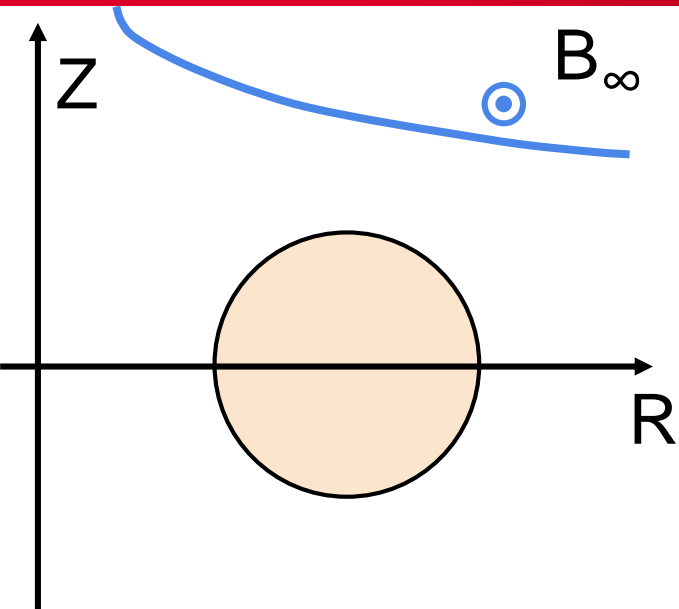
✦ Homogenization : deposited matter leads to a new axisymmetric density and temperature profiles



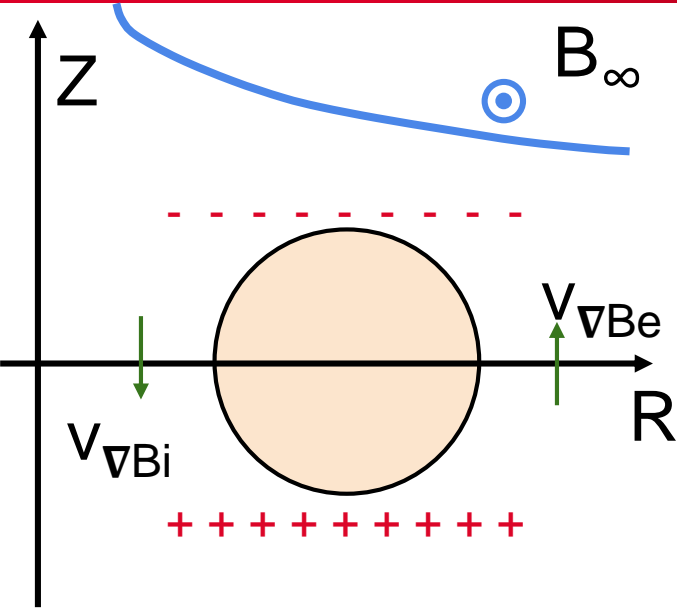
✦ Deposited matter displacement :

⇒ Parallel expansion

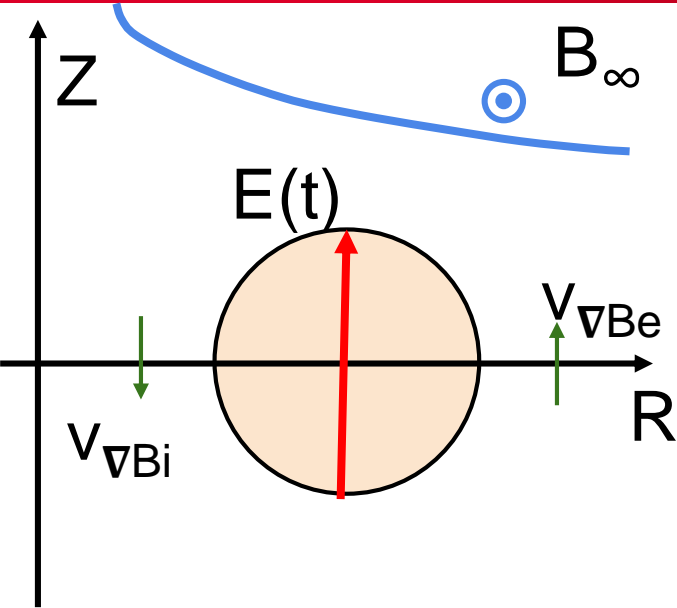
⇒ **Radial drift** (down  $\nabla B$  direction)



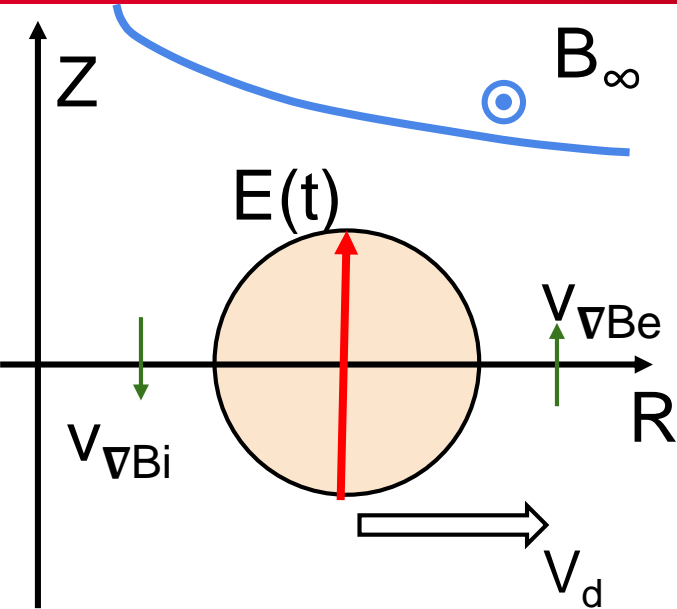




$V_{\nabla B_{e,i}}$  : Vertical  $e^-$ ,  $i^+$  drift

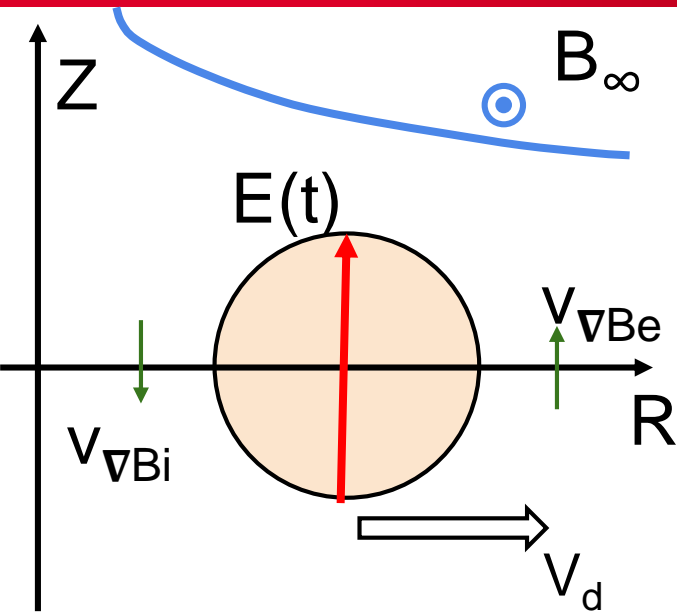


$V_{\nabla B_{e,i}}$  : Vertical  $e^-$ ,  $i^+$  drift



$V_{\nabla B_{e,i}}$  : Vertical  $e^-$ ,  $i^+$  drift

$$V_d = \frac{E \times B_\infty}{B_\infty^2}$$



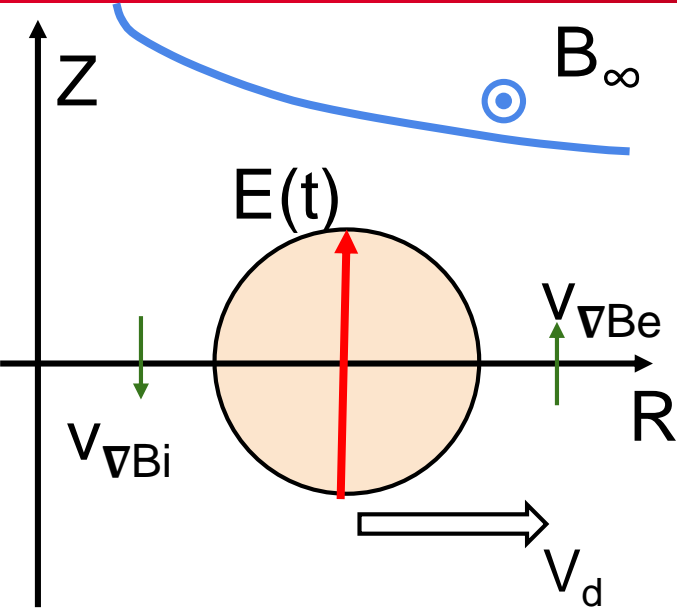
$\mathbf{V}_{\nabla B_{e,i}}$  : Vertical  $e^-$ ,  $i^+$  drift

$$V_d = \frac{\mathbf{E} \times \mathbf{B}_{\infty}}{B_{\infty}^2}$$

We can calculate the drift acceleration :

$$\frac{dV_d}{dt} = \frac{2(p_0 - p_{\infty})}{n_0 m_0 R_c}$$

$p_0$  : Ionised cloud pressure  
 $p_{\infty}$  : Background plasma pressure  
 $n_0$  : Ionised cloud density  
 $m_0$  : Ionised cloud mass  
 $R_c$  : Curvature radius

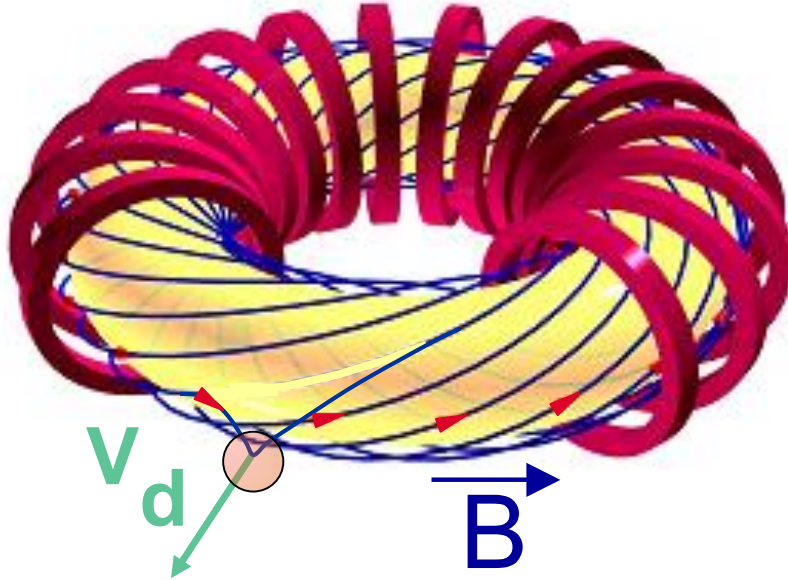


$\mathbf{V}_{\nabla B_{e,i}}$  : Vertical  $e^-$ ,  $i^+$  drift

$$V_d = \frac{\mathbf{E} \times \mathbf{B}_{\infty}}{B_{\infty}^2}$$

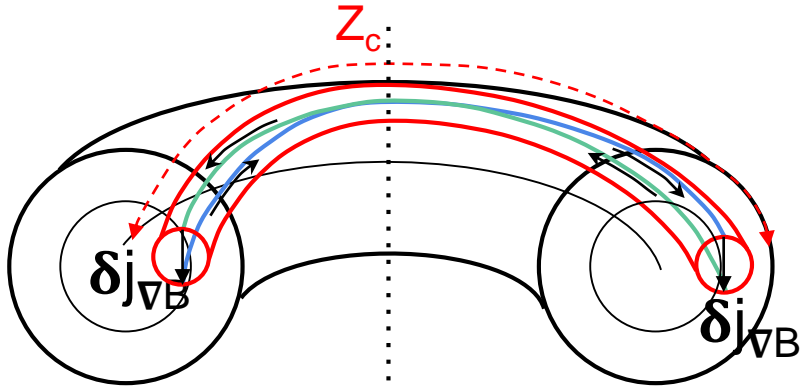
We can calculate the drift acceleration :

$$\frac{dV_d}{dt} = A_{\nabla B}$$



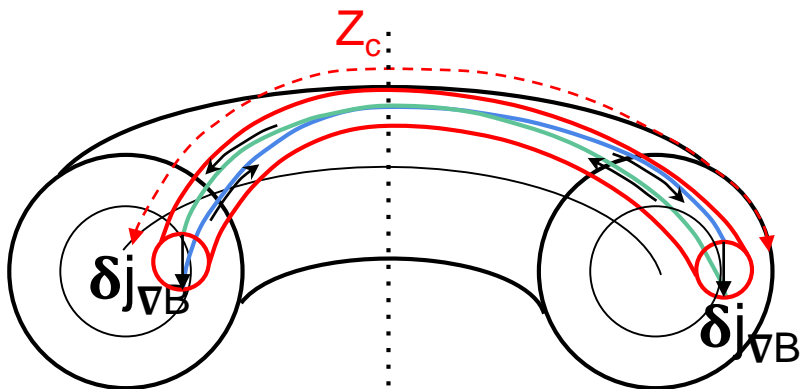
✦ Ideal MHD :  
Cloud drags magnetic flux tube

✦ Rotational transform, winding of the field line  
⇒ Drift damping by 2 phenomena



- ✦ Critical length  $Z_c$  reach  
→ drift current circuit is closed inside the cloud

[Rozhansky 2005]



[Rozhansky 2005]

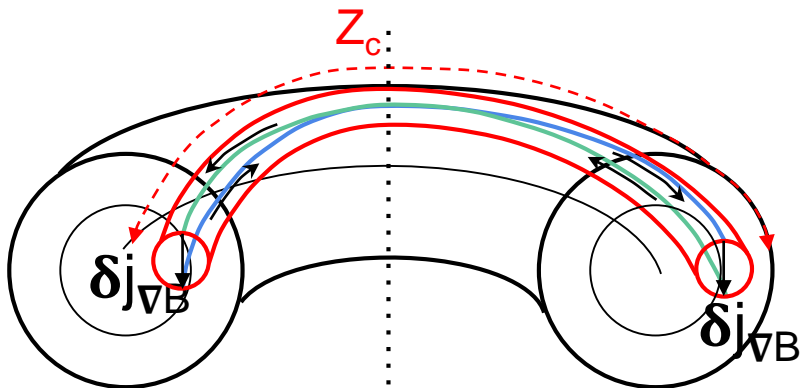
$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC}$$



1<sup>st</sup> damping term

→ Internal **C**onnection





[Rozhansky 2005]

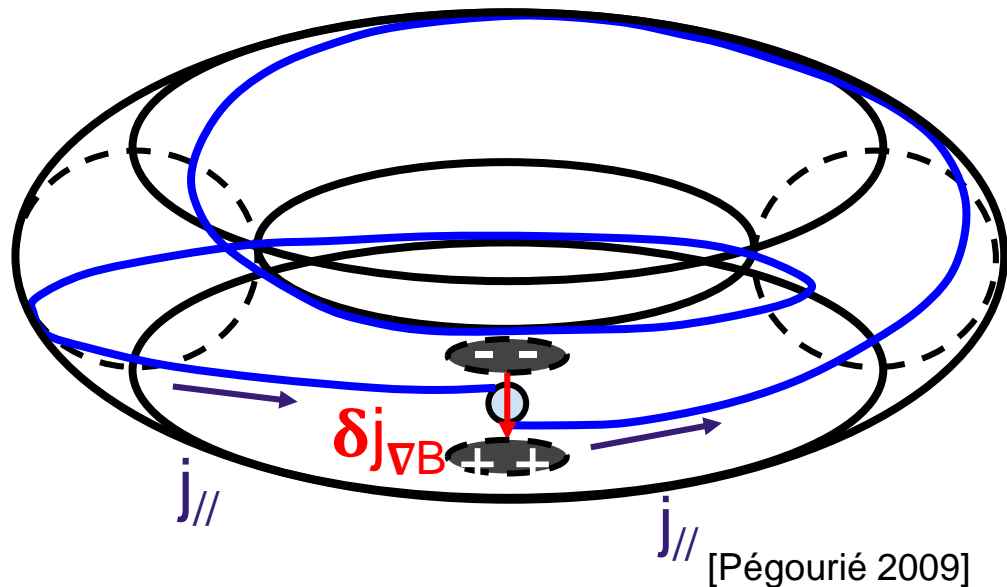
$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} \mathcal{D}_{IC} \propto \mathcal{H}(Z_c - Z_0)$$



1<sup>st</sup> damping term  
→ **I**nternal **C**onnection

$Z_c$  : Critical length where the relative current are inverted  
 $Z_0$  : Cloud length

Parallel currents flow along field lines  
→ closing drift current

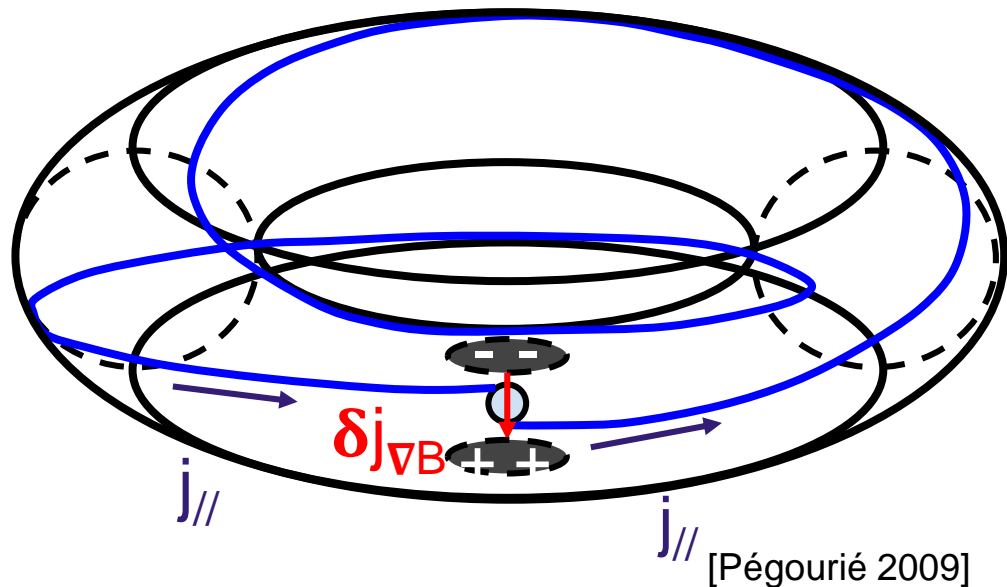


$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC} - D_{EC}$$




2<sup>nd</sup> damping term

→ **External Connection**

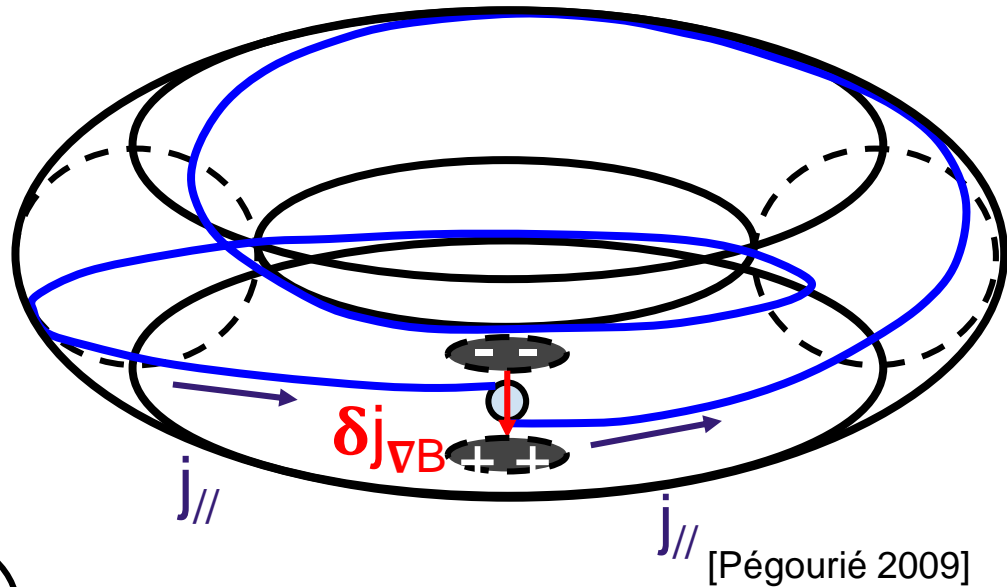


$\sigma_{\infty}$  : Parallel conductivity  
 $Z_{\infty}$  : Length of the connecting flux tube

$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC} - \textcircled{D_{EC}}$$

 2<sup>nd</sup> damping term  
 → **External Connection**

$$\propto V_d \frac{\sigma_{\infty} B_{\infty}^2}{Z_{\infty}}$$

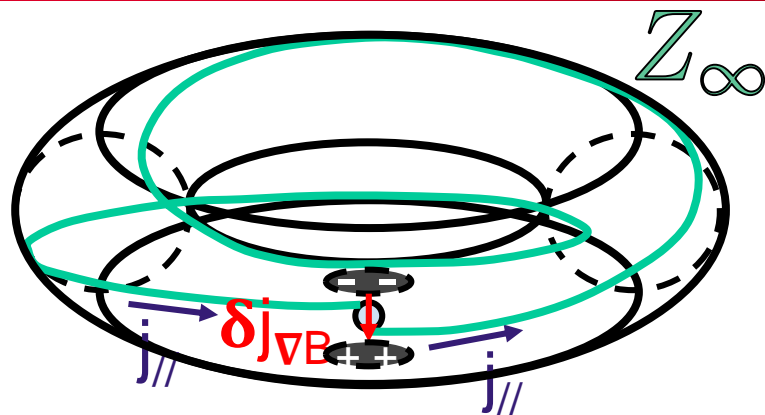


$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC} - D_{EC}$$

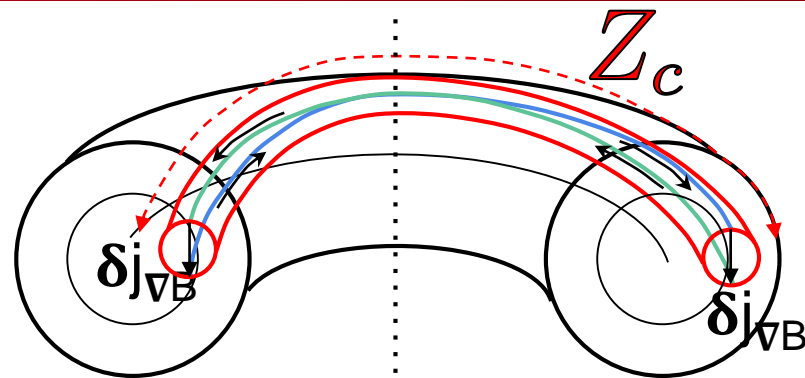
$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC} - D_{EC}$$

How  $D_{EC}$  &  $D_{IC}$  influence the deposition profile for different magnetic configuration ? (tokamak/Stellarator/RFP)

# Competition between $D_{EC}$ & $D_{IC}$ - in a tokamak the external connection is the dominant effect



$$\tau_{EC} \sim \frac{Z_\infty}{C_A}$$



$$\tau_{IC} \sim \frac{Z_c}{C_s}$$

$\tau$  : efficient time

$$C_A \gg C_s$$

$$Z_\infty > Z_c$$

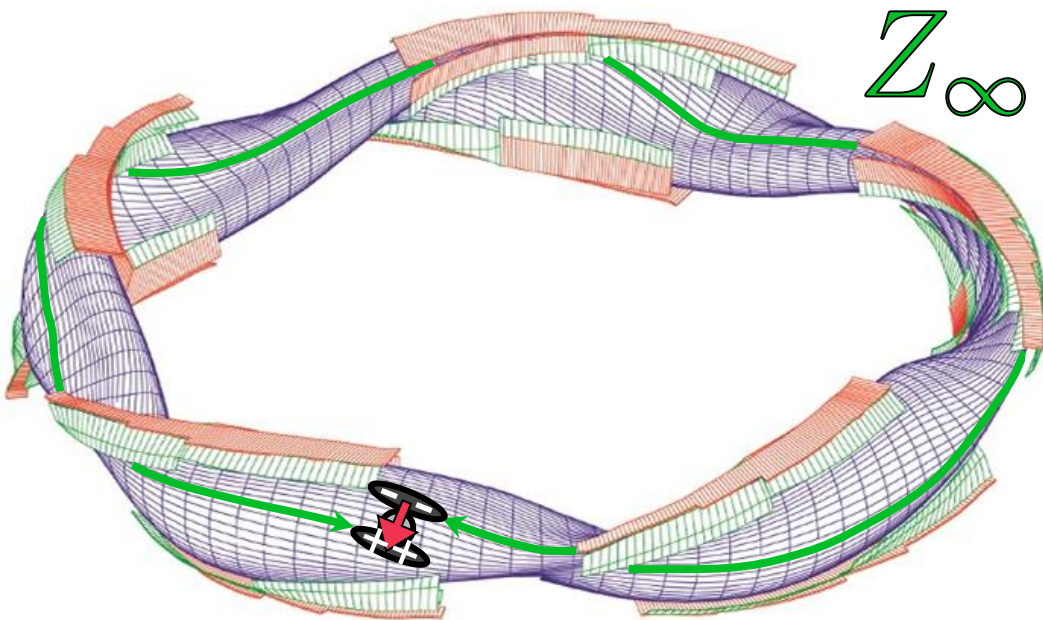
More efficient close to a rational  $q$

$$\tau_{EC} \sim \frac{Z_{\infty}}{C_A} < \tau_{IC} \sim \frac{Z_c}{C_s}$$

[Sakamoto 2013]

$\Rightarrow$  External Connection  
more efficient for tokamak

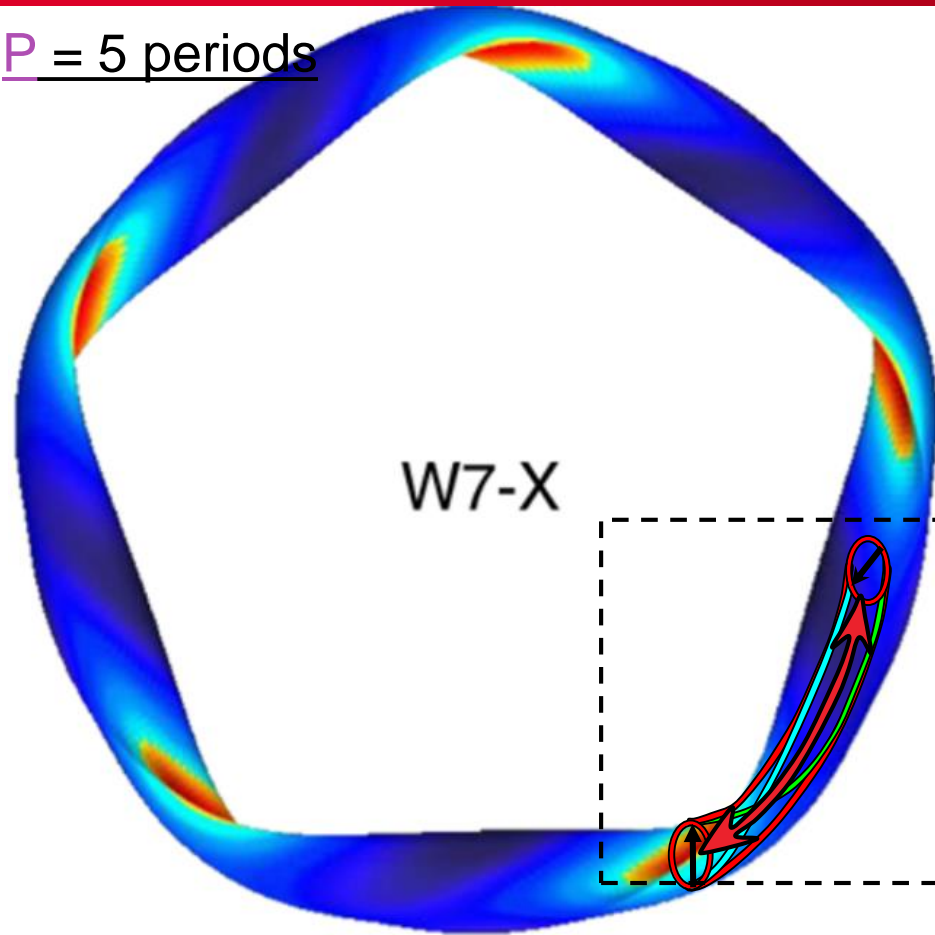




$$\tau_{EC} \sim \frac{Z_\infty}{C_A}$$

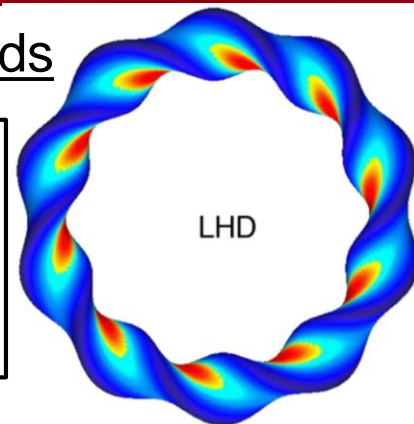
# Competition between $D_{EC}$ & $D_{IC}$ - in a stellarator; Internal Connection

$P = 5$  periods



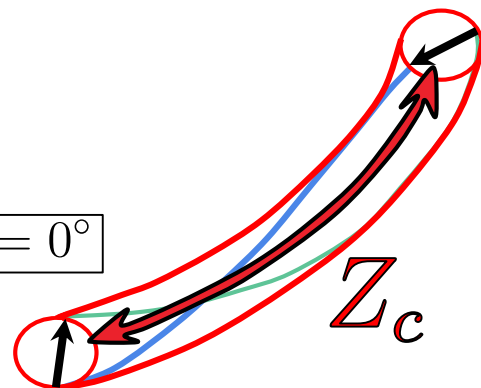
$P = 10$  periods

$$\tau_{IC} \sim \frac{Z_c(P)}{C_s}$$



$$\phi = 0^\circ$$

$$\phi = \frac{\pi}{P}^\circ$$



$$\tau_{EC} \sim \frac{Z_{\infty}}{C_A} > \tau_{IC} \sim \frac{Z_c(P)}{C_s}$$

[Matsuyama 2012]

⇒ **Internal Connection** more  
efficient for stellarator

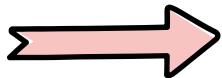
We have :

$$\star \tau_{EC} \text{ tokamak} \sim \tau_{EC} \text{ stellarator}$$

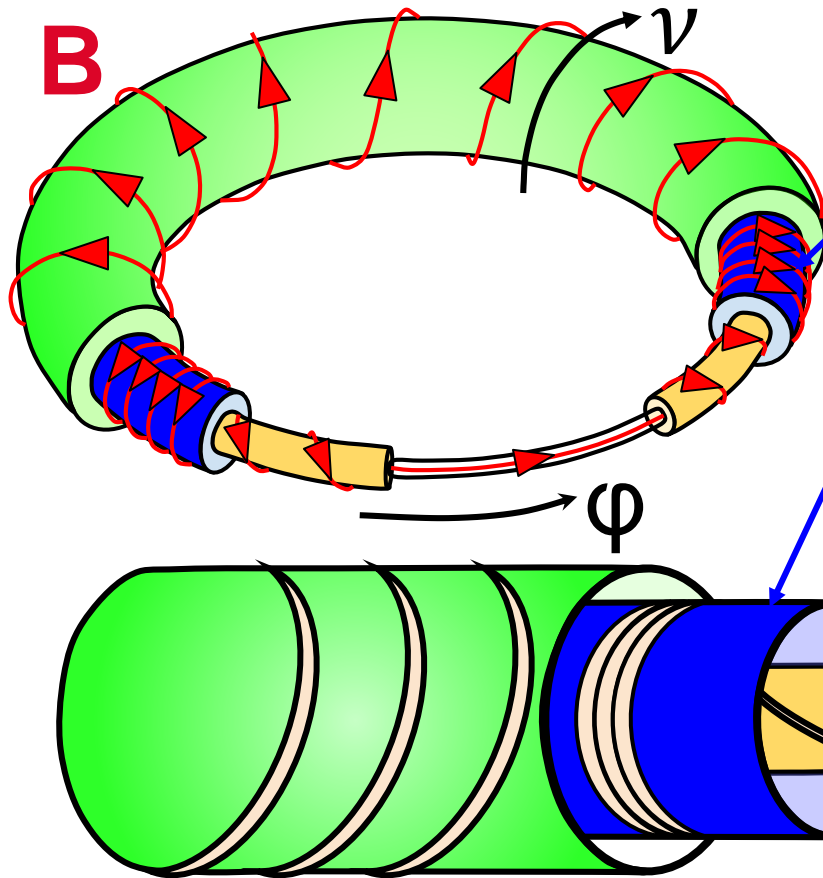
$$\star \tau_{EC} \text{ tokamak} < \tau_{IC} \text{ tokamak} \quad \& \quad \tau_{EC} \text{ stellarator} > \tau_{IC} \text{ stellarator}$$

Then :

$$\Rightarrow \tau_{EC} \text{ tokamak} > \tau_{IC} \text{ stellarator}$$



**Drift displacement is smaller in a stellarator than in tokamak**



At the reversal radius :

$$\left. \begin{aligned} \tau_{Ec} &= \frac{2\pi a}{C_A} \\ \tau_{IC} &= \frac{\pi a}{C_s} \end{aligned} \right\} \tau_{RFP} \propto a$$

$$\neq$$

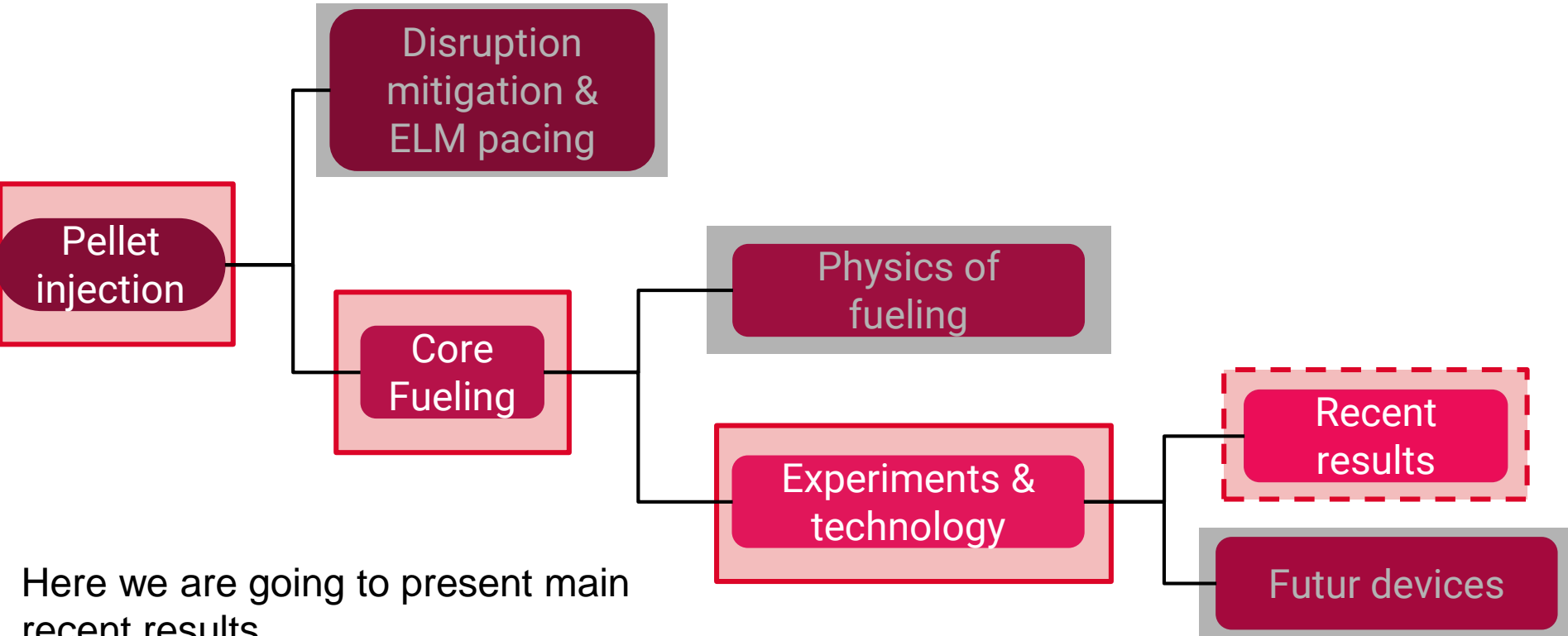
$$\tau_{\text{tokamak, stellarator}} \propto R$$

$\Rightarrow \tau_{RFP} \ll \tau_{\text{tokamak, stellarator}}$   
 $\Rightarrow$  Very short drift time: magnetic shear

$\Rightarrow$  Drift barrier

[Canton 2000]

No experiments made yet

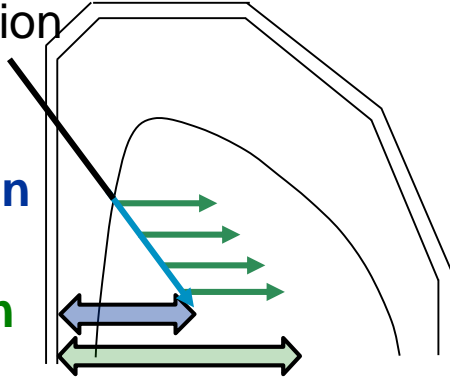


Here we are going to present main recent results  
 ⇒ Similar results on other machines also exist

# I - Better fueling from High field side in DIII-D due to the drift of the cloud

Pellet injection

Penetration  
length  
Deposition  
length



✦ Matter deposition deeper than pellet penetration :  
⇒ Drift of the cloud

[Baylor 2007]

(ablation of the  
pellet)

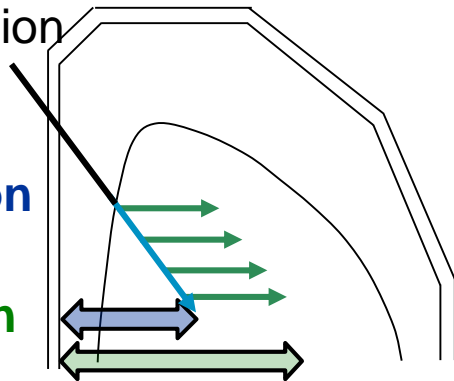
(drift of the  
cloud)

# I - Better fueling from High field side in DIII-D due to the drift of the cloud

Pellet injection

Penetration length

Deposition length

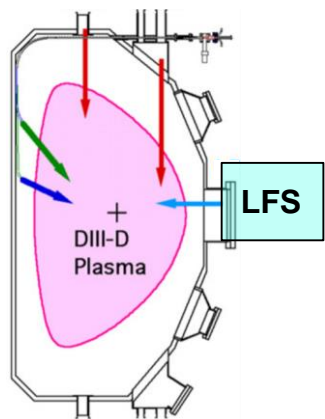


✦ Matter deposition deeper than pellet penetration :  
⇒ Drift of the cloud

✦ Test of different injection points :

**LFS** : Deposition ~ penetration

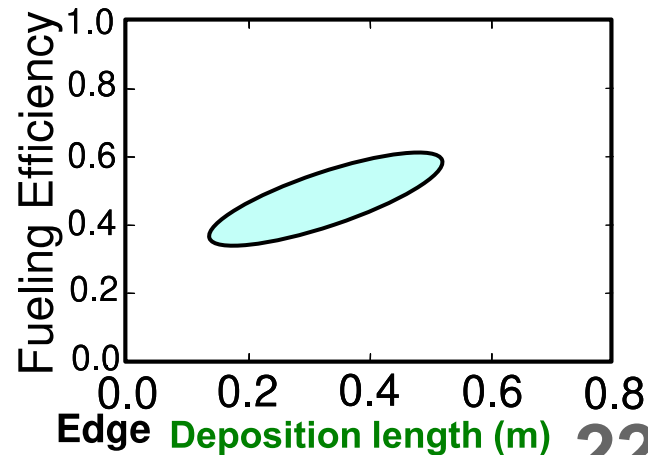
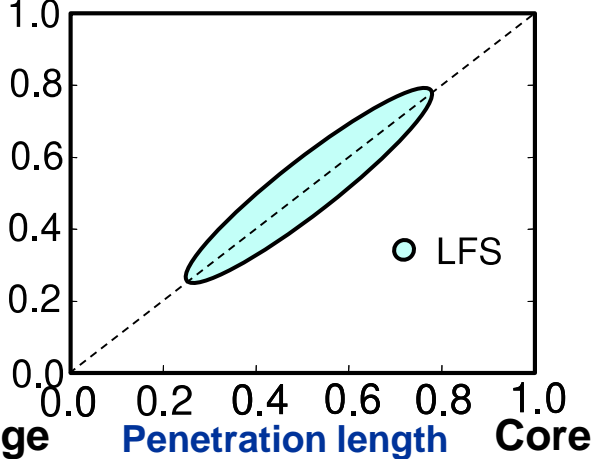
[Baylor 2007]



Core

Deposition length

Edge



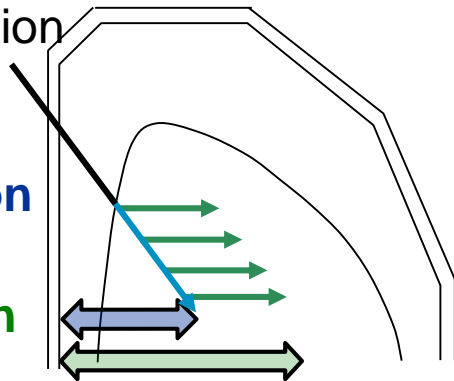


# I - Better fueling from High field side in DIII-D due to the drift of the cloud

Pellet injection

Penetration length

Deposition length

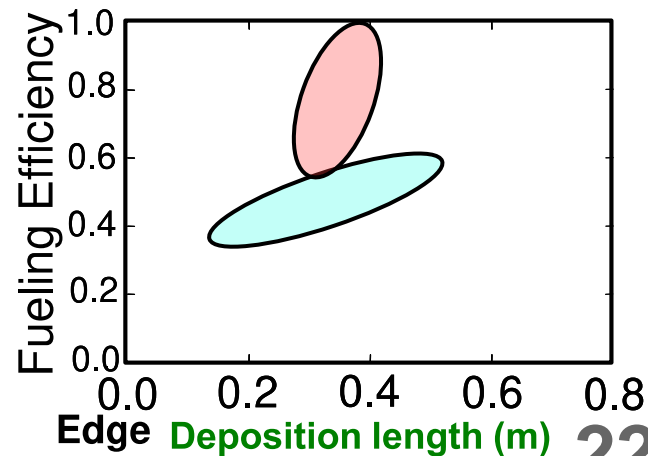
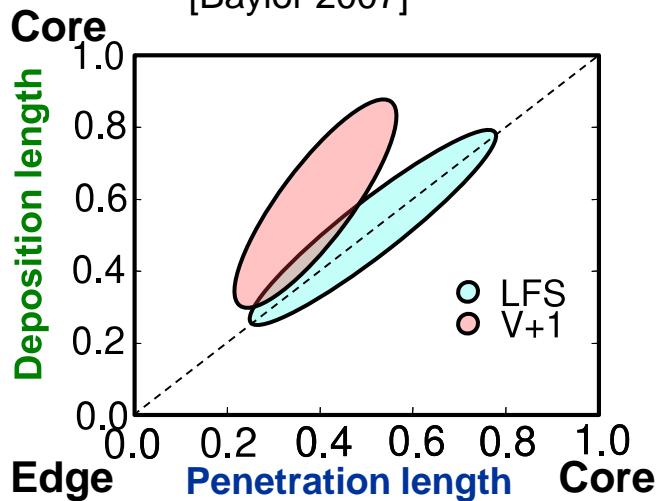
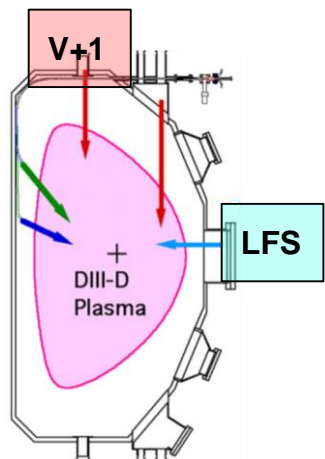


✦ Matter deposition deeper than pellet penetration :  
⇒ Drift of the cloud

✦ Test of different injection points :

LFS	: Deposition ~ penetration
V+1	: Deposition ~ 2 x deeper than penetration

[Baylor 2007]

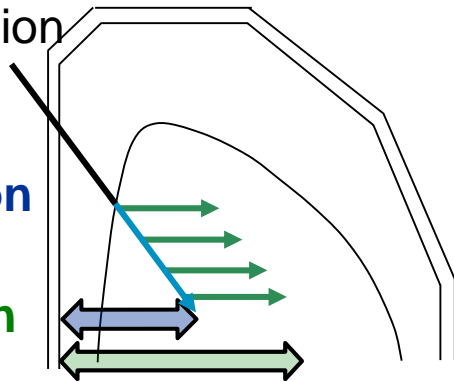


# I - Better fueling from High field side in DIII-D due to the drift of the cloud

Pellet injection

Penetration length

Deposition length

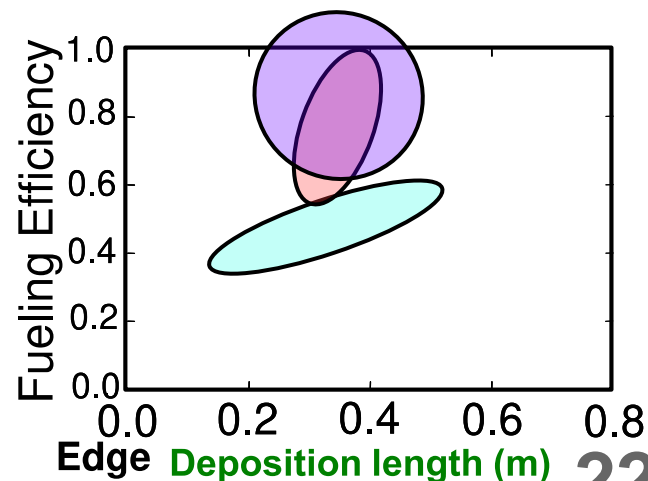
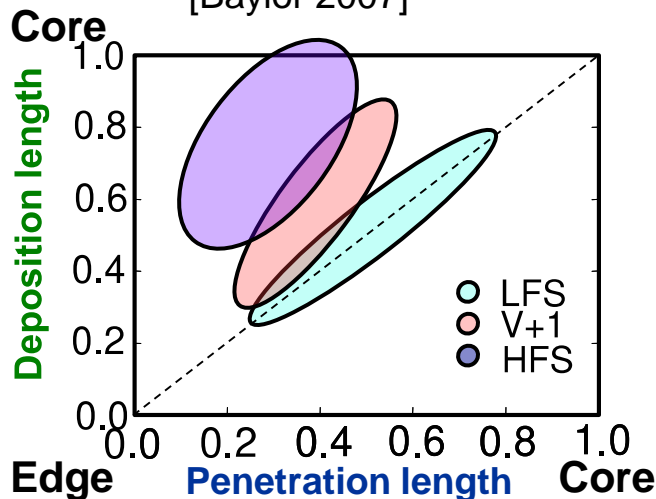
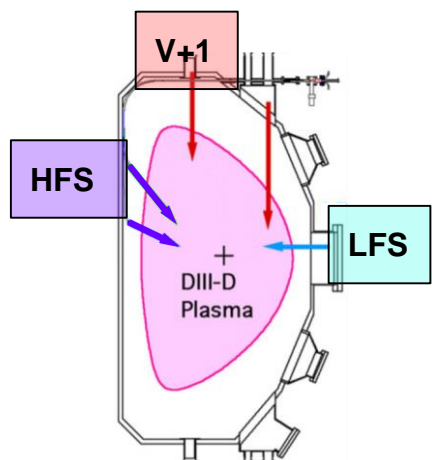


✦ Matter deposition deeper than pellet penetration :  
⇒ Drift of the cloud

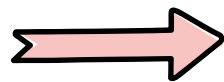
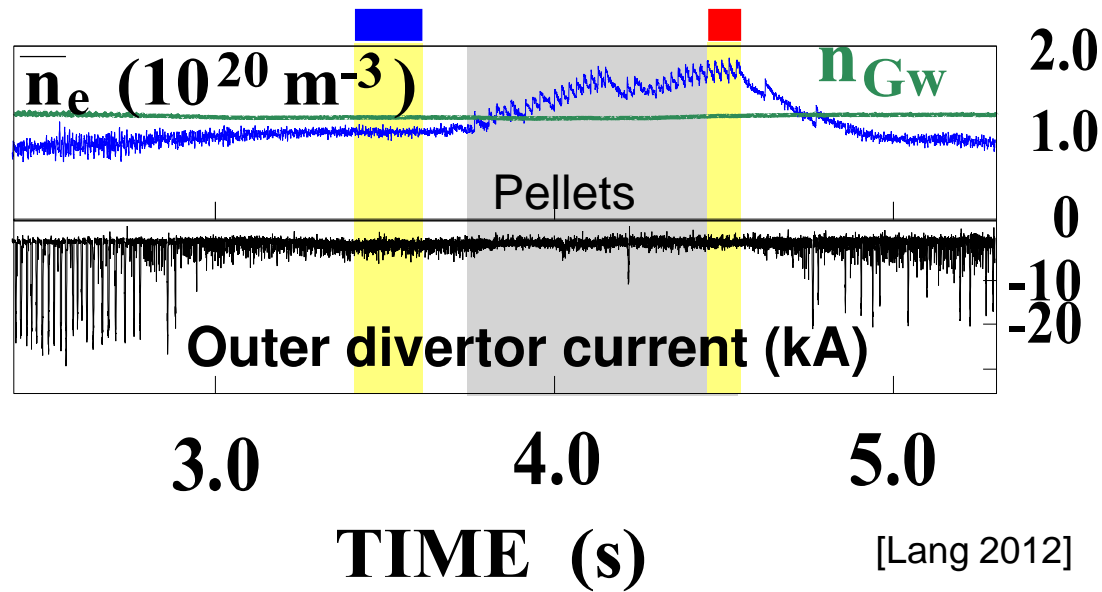
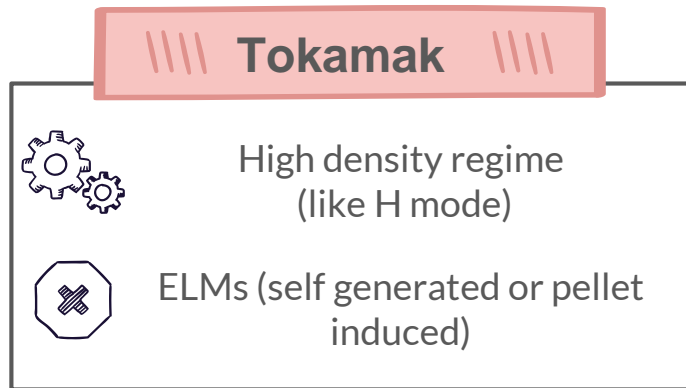
✦ Test of different injection points :

LFS	:	Deposition ~ penetration
V+1	:	Deposition ~ 2 x deeper than penetration
HFS	:	Deposition ~ 4 x deeper than penetration

[Baylor 2007]



## II- Pellet fueling allows RMP ELM suppression above Greenwald density in ASDEX-Upgrade



Resonant Magnetic Perturbation (RMP) + Pellet allowed a density  $> n_{GW}$  without ELM

## Stellarator

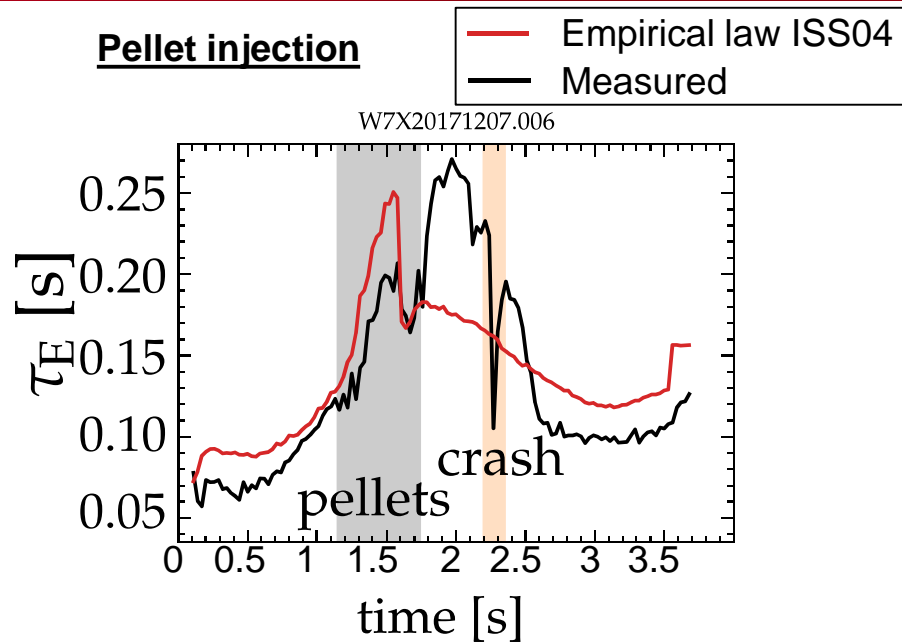


- High density regime
- Large confinement time



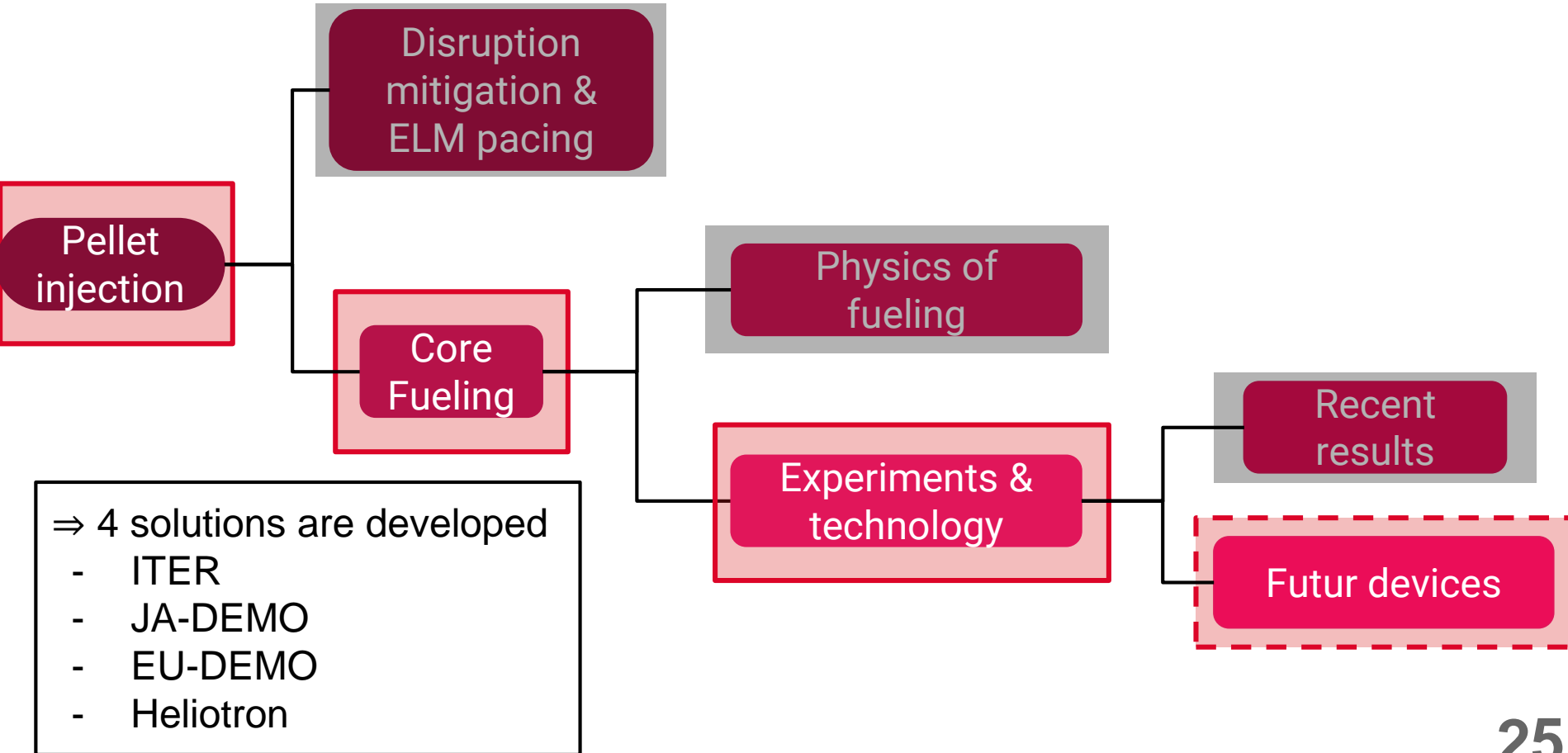
- Hollow density profile

### Pellet injection



[Balazukov 2018]

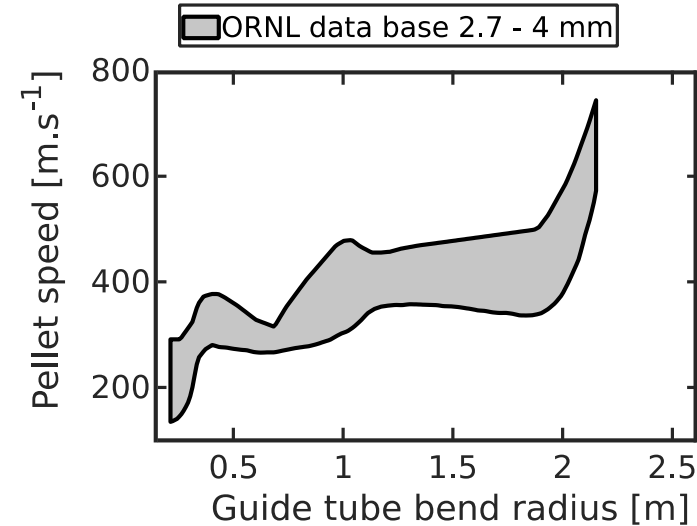
- ✦ Pellet increases core density
- ✦ Pellet increases global energy confinement time



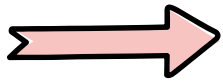
Futur devices will be large

- Large drift
- injection from HFS
- Bended guide tube
- Limited pellet speed  $V_p^{\text{Max}}$

$R_p$  (pellet radius) limited by plasma perturbation



[Poeckl 2021]



Balance to find between  $R_p$  &  $V_p^{\text{Max}}$   
Futur machines take into account pellet injector position

## 5 fueling system dimensioned :

### 2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

### 2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

### 1 preliminary state :

FFHR (stellarator)

## 5 fueling system dimensioned :

### 2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

### 2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

### 1 preliminary state :

FFHR (stellarator)



## 5 fueling system dimensioned :

### 2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

### 2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

### 1 preliminary state :

FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO
Fueling rate	$\leq 62\text{mg/s}$	$\in [20,167]\text{mg/s}$	$50\text{mg/s}$	$\in [42,58]\text{mg/s}$

## 5 fueling system dimensioned :

### 2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

### 2 as project :

JA-DEMO (tokamak)

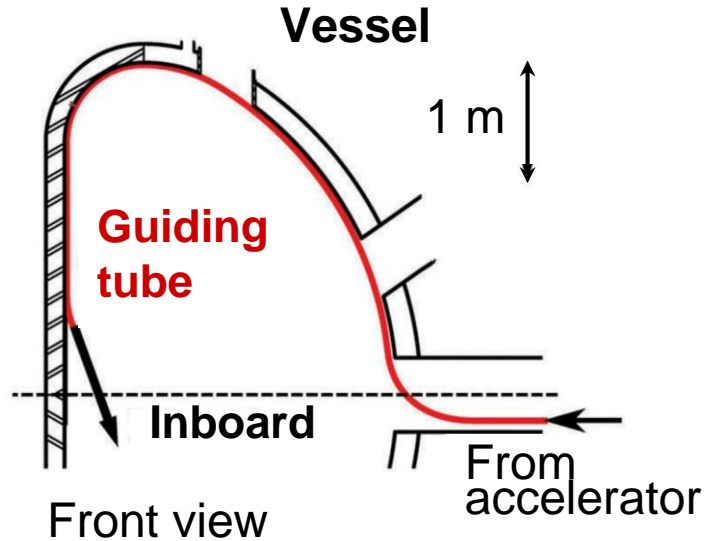
EU-DEMO (tokamak)

### 1 preliminary state :

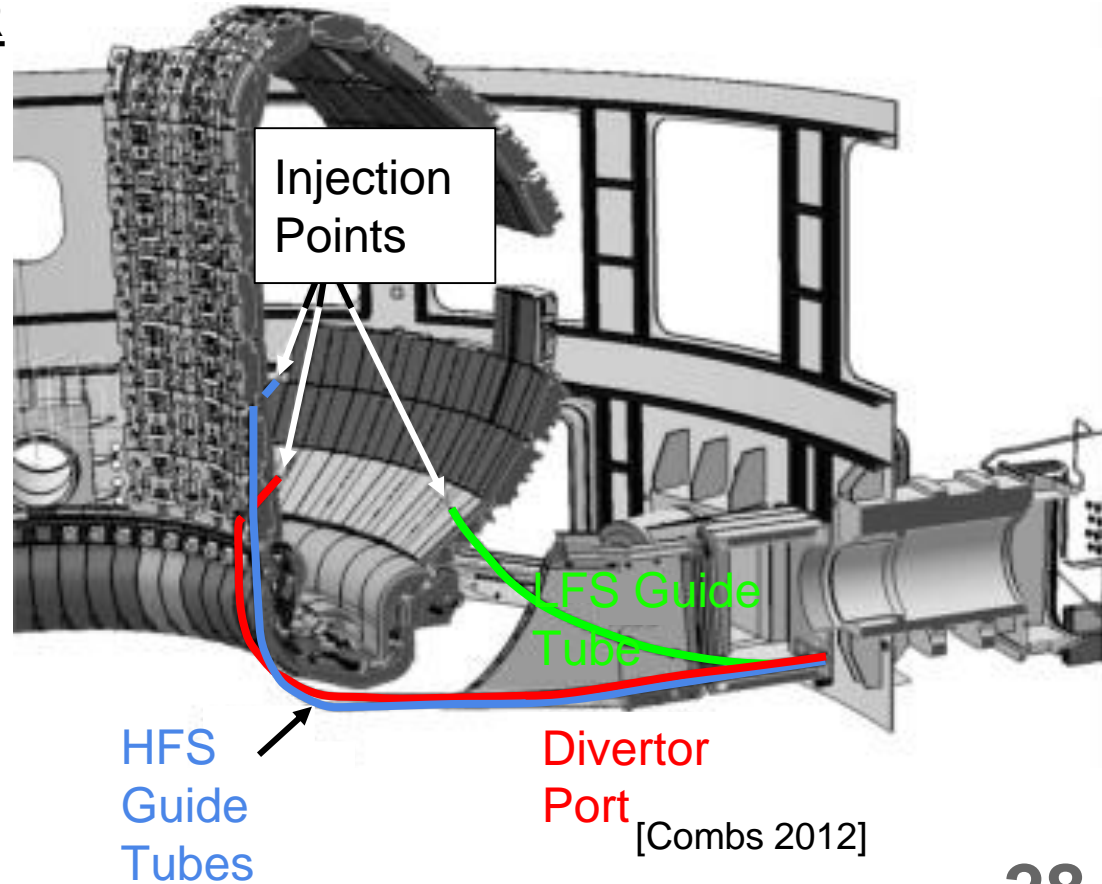
FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO
Fueling rate	$\leq 62\text{mg/s}$	$\in [20,167]\text{mg/s}$	$50\text{mg/s}$	$\in [42,58]\text{mg/s}$
Pellet Size	$\in [1,5]\text{mg}$ $\in [2,3]\text{mm}$	<b>25mg</b> <b>5mm</b>	<b>17mg</b> <b>4mm</b>	<b>8mg</b> <b>3.4mm</b>

## JT-60SA



## ITER



[Lang 2019]

- Midplane or bottom injector
- strong tube bend

## 5 fueling system dimensioned :

2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

2 as project :

JA-DEMO (tokamak)

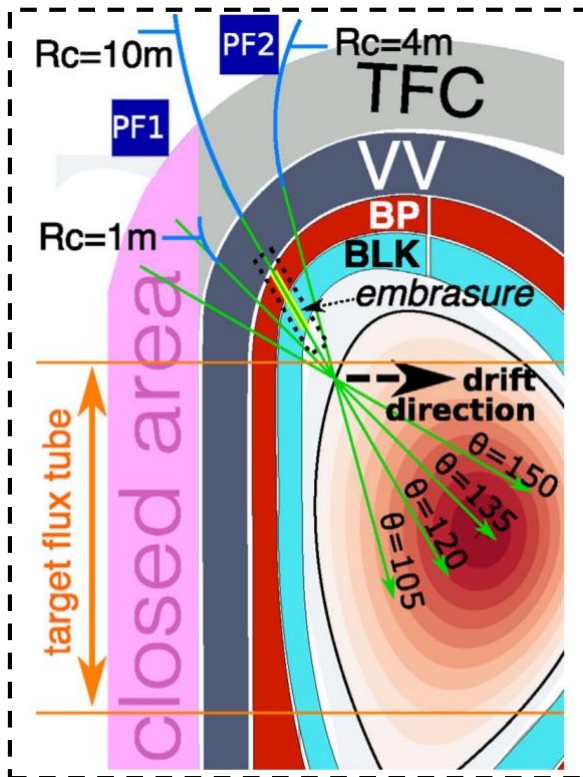
EU-DEMO (tokamak)

1 preliminary state :

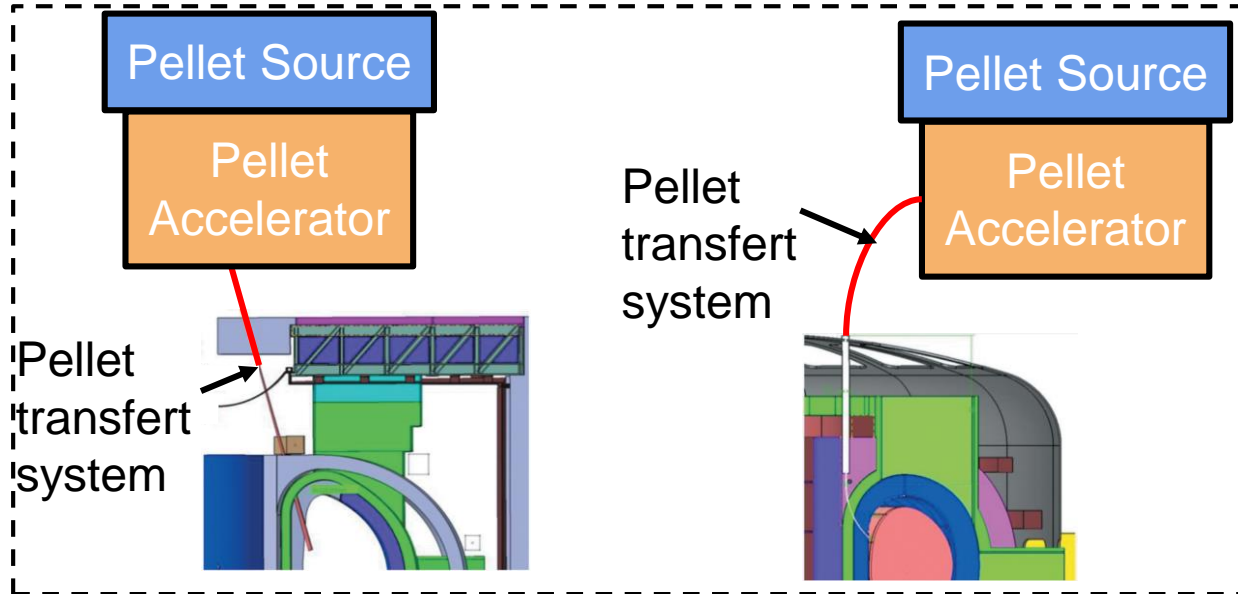
FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO
Injector position	midplane	midplane - bottom		
Injection lines	small $R_c$	small $R_c$		
$V_p^{Max}$	470 m/s	300 m/s		
Injector type	centrifuge	1 stage pneumatic		

## JA-DEMO



## EU-DEMO



[Poeckl 2021]

[Tokugana 2017]

## 5 fueling system dimensioned :

### 2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

### 2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

### 1 preliminary state :

FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO	
Injector position	midplane	midplane - bottom	top	top	
Injection lines	small $R_c$	small $R_c$	Large $R_c$	Large $R_c$	
$V_p^{Max}$	470 m/s	300 m/s	2000m/s	1700m/s	3000m/s
Injector type	centrifuge	1 stage pneumatic	2 stage pneumatic	centrifuge - 1 stage pneumatic	2 stage pneumatic

## 5 fueling system dimensioned :

### 2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

### 2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

### 1 preliminary state :

FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO		FFHR
Fueling rate	$\leq 62\text{mg/s}$	$\in [20,167]\text{mg/s}$	50mg/s	$\in [42,58]\text{mg/s}$		200 mg/s
Pellet Size	$\in [1,5]\text{mg}$ $\in [2,3]\text{mm}$	25mg 5mm	17mg 4mm	8mg 3.4mm		40-60mg 5.6mm
$V_p^{\text{Max}}$	470 m/s	300 m/s	2000m/s	1700 m/s	3000 m/s	10 000 m/s

Speed not possible to reach yet



	JT-60SA	ITER	JA-DEMO	EU-DEMO		FFHR
Fueling rate	$\leq 62\text{mg/s}$	$\in [20,125]\text{mg/s}$	$50\text{mg/s}$	$\in [42,58]\text{mg/s}$		<b>600 mg/s</b>
Pellet Size	$\in [1,5]\text{mg}$ $\in [2,3]\text{mm}$	25mg 5mm	17mg 4mm	8mg 3.4mm		40-60mg 5.6mm
$V_p^{\text{Max}}$	470 m/s	300 m/s	2000m/s	1700 m/s	3000 m/s	1200 m/s

**Not possible to increase pellet size**

⇒ unacceptable jumps in fusion power & heat loads of the divertor

- ✦ Understand **Ablation and Homogenization physic** let us understand differences for tokamak/stellarator/RFP



- ✦ Fuelling using pellets allows **high performance discharges**

## Tokamak

- $> n_{gw}$  without ELMs

## Stellarator

- $\tau_E \nearrow$
- Peak density profil



- ✦ **Pellet injection line** to be considered from **very early stage** of the design of future devices.

- allows better fuelling efficiency
- reduced fuelled circulation