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OXIDATION OF A COLD-WORKED 316L STAINLESS STEEL IN PRESSURIZED WATER REACTOR PRIMARY WATER ENVIRONMENT

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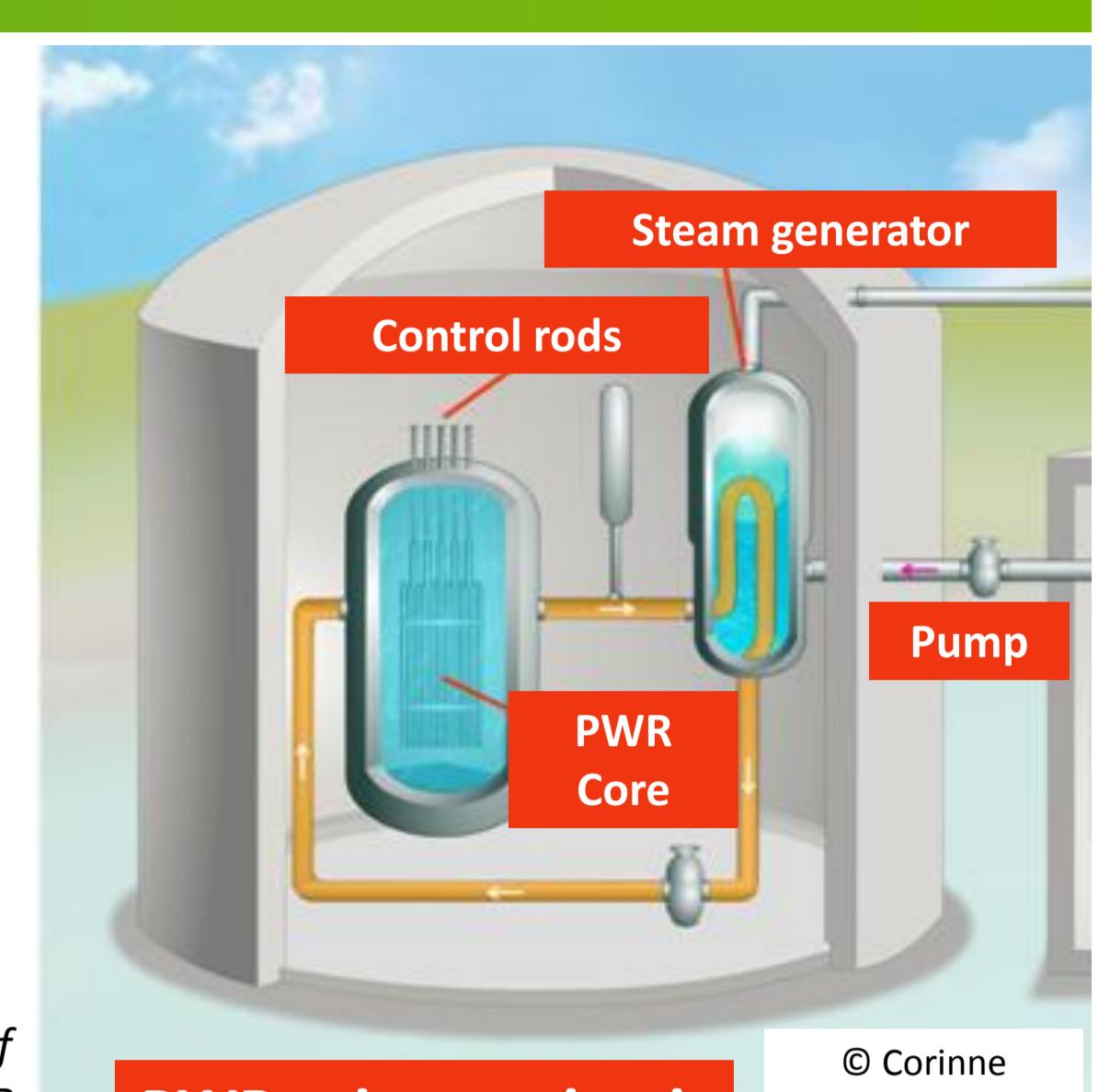
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Introduction

- Pressurized Water Reactors (PWR) represent 76.3 % of the electrical power produced in 2015 in France [1]
- Operational feedback → intergranular Stress Corrosion Cracking (SCC)** affecting cold-worked stainless steel components in PWR primary water [2]
- PWR primary water : pure hydrogenated and deaerated water, with Li and B additions, 150 bars and 290-340 °C
- Oxygen transients** (oxygen injections in PWR primary water [3, 4]) = Possible detrimental factor
- Dissolved oxygen in PWR primary water has an impact on the :
 - Location of initiation sites (trans- or intergranular sites) [5]
 - Oxide layer properties (inner layer morphology and composition) [6]
- However, the oxygen transient effect on SCC susceptibility has not been extensively investigated to date



Schematic representation of the primary circuit of a PWR

PWR primary circuit

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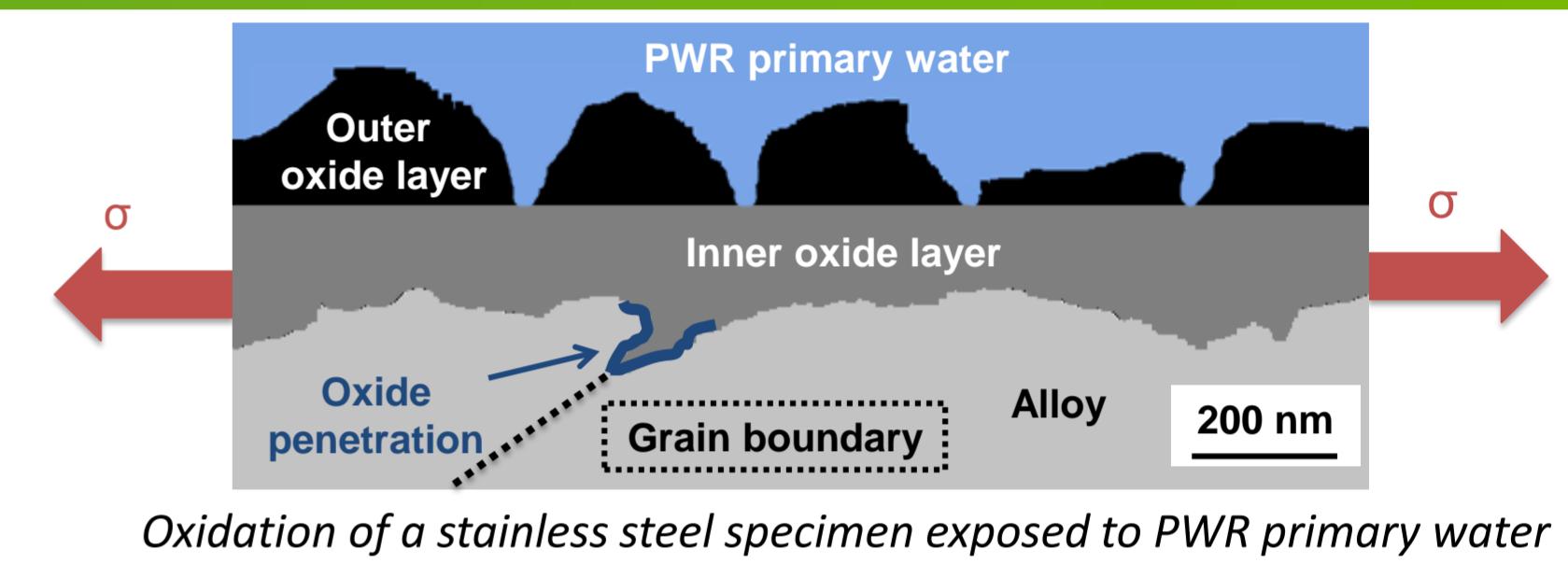
Objectives

General aim: Determine the effect of dissolved oxygen on SCC susceptibility of a cold-worked stainless steel in PWR primary water

- Hypothesis: Link between oxidation and SCC susceptibility
- In particular, localized oxide penetrations are suspected to play a crucial role in crack initiation

First step: effect of dissolved oxygen in PWR primary water

- On oxidation kinetics and surface oxide layers nature
- On localized oxide penetration kinetics, morphology and nature



Pre-strained / non cold-worked 316L stainless steel specimens

Material and Experimental Conditions

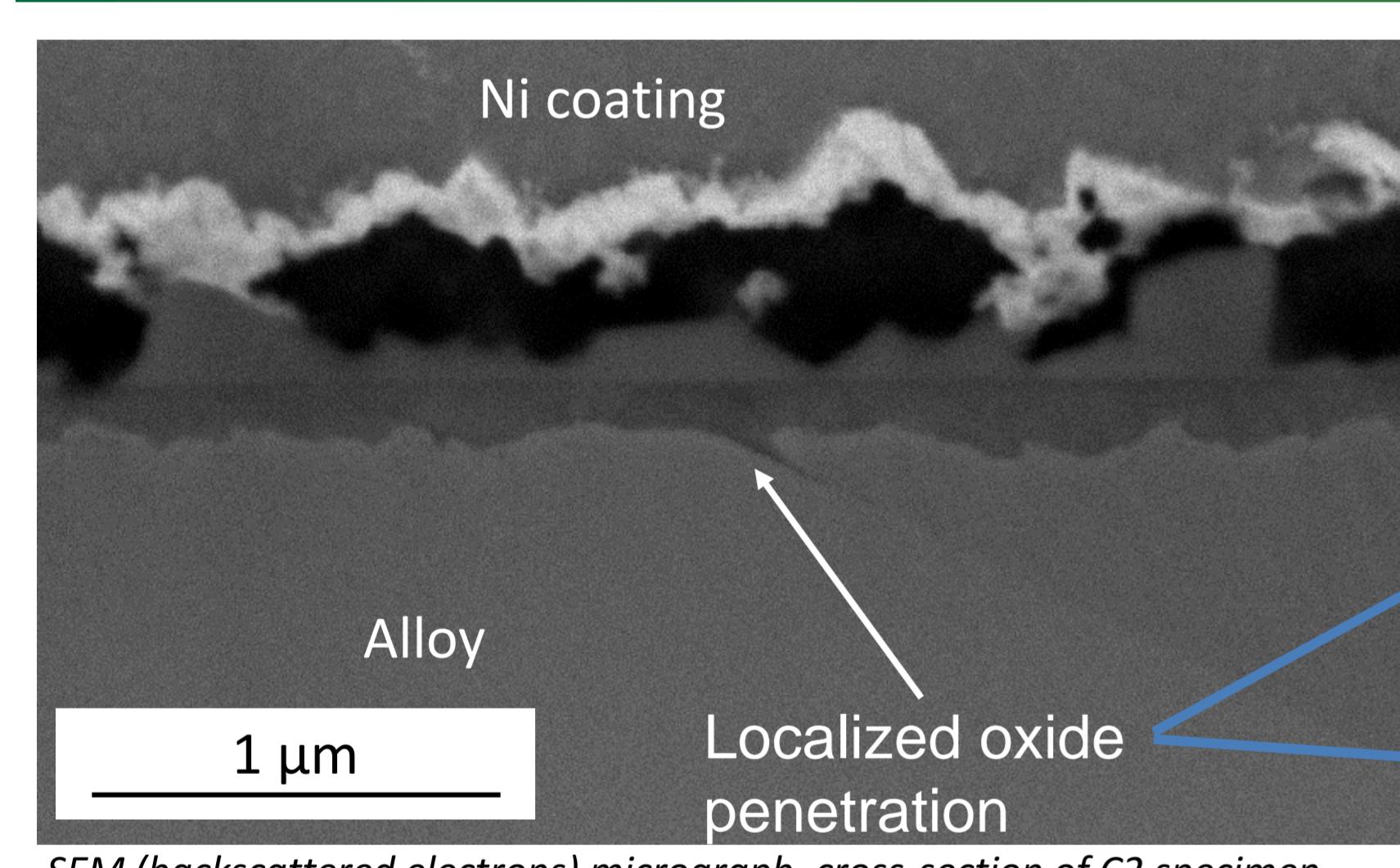
Composition (weight %)	C	S	P	Si	Mn	Ni	Cr	Mo	Cu	N
316L – this study	0,016	0,0009	0,026	0,62	1,86	10	16,54	2,03	-	0,022

Annealing treatment (1050°C, Ar overpressure, 1h) applied to our specimens

→ Isotropic austenite grains ($50 \pm 10 \mu\text{m}$) and residual ferrite (1-5 % in volume)

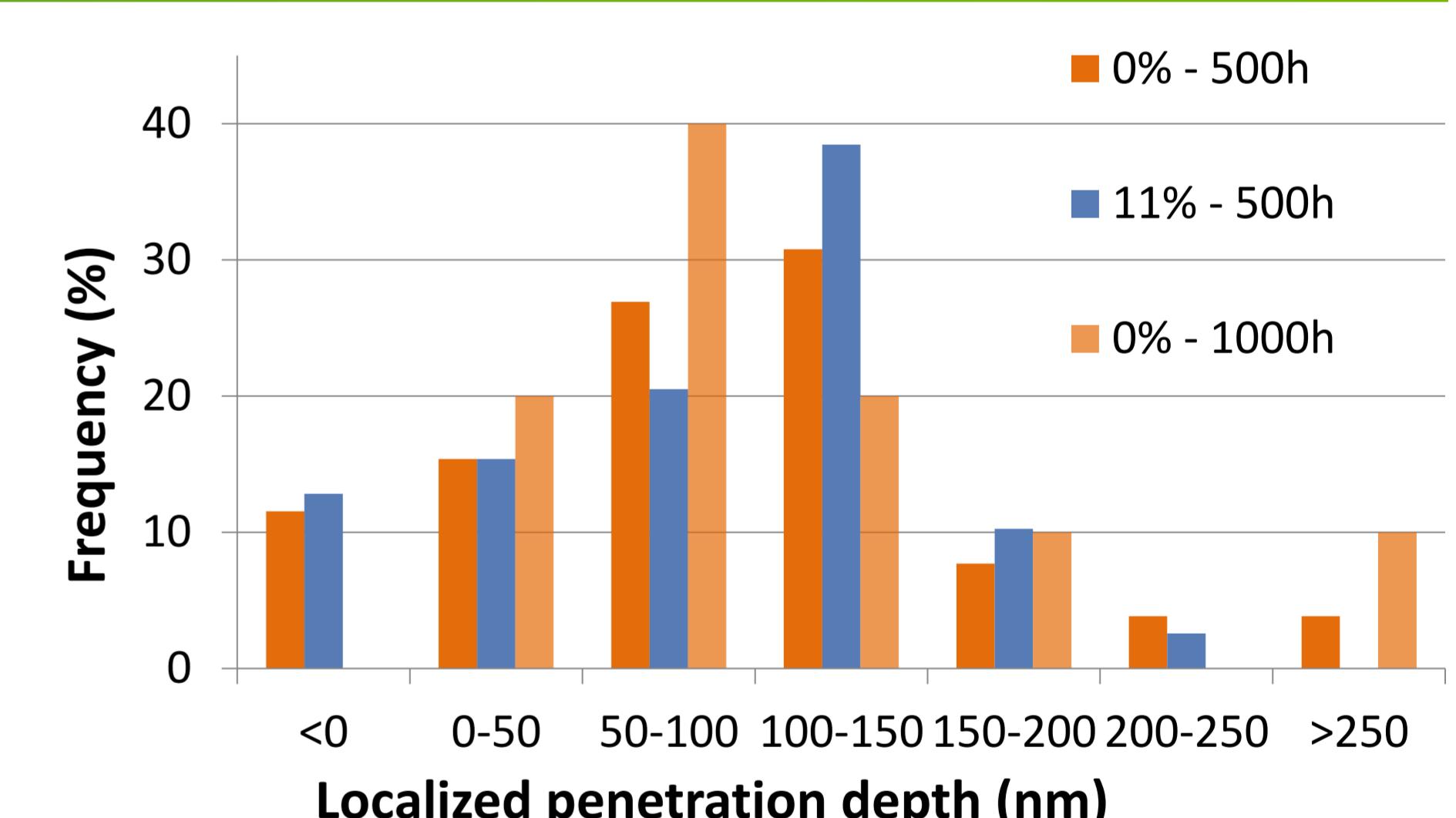
→ Non-sensitized material

Nominal PWR primary water (pure water, 150 bars, 340°C, pH = 7.0 to 7.2)					
Element	B	Li	H	O	
Concentration	1000 ppm	2 ppm	25-35 mL/kg (TPN)	< 0,01 ppm	
Chlorides, sulfates, fluorides					
Oxidation in nominal PWR primary water	C2 Oxidation time = 500 h Non cold-worked	C1 Oxidation time = 1000 h Non cold-worked	EP1 Oxidation time = 500 h Pre-strained (11%)		

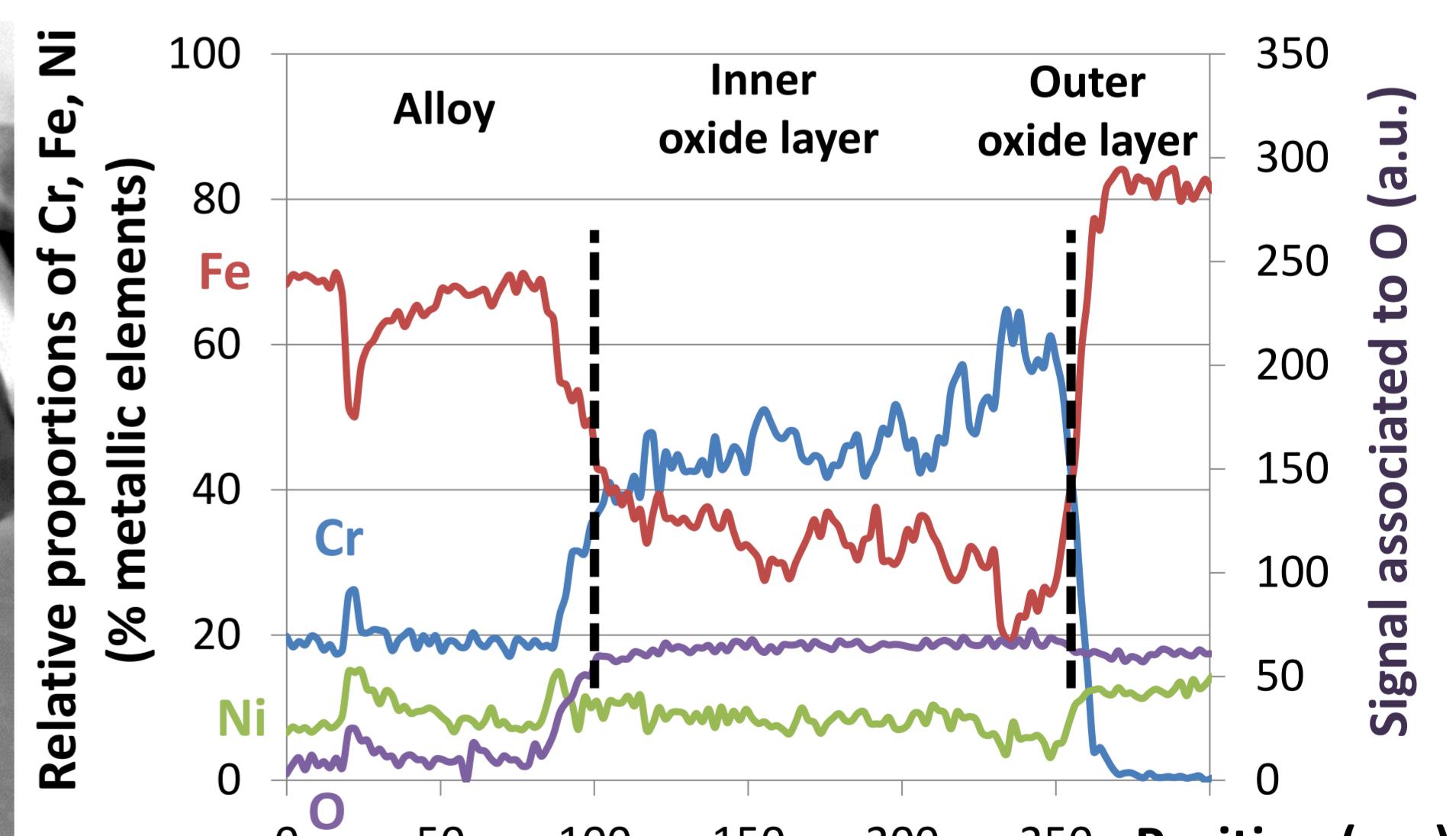
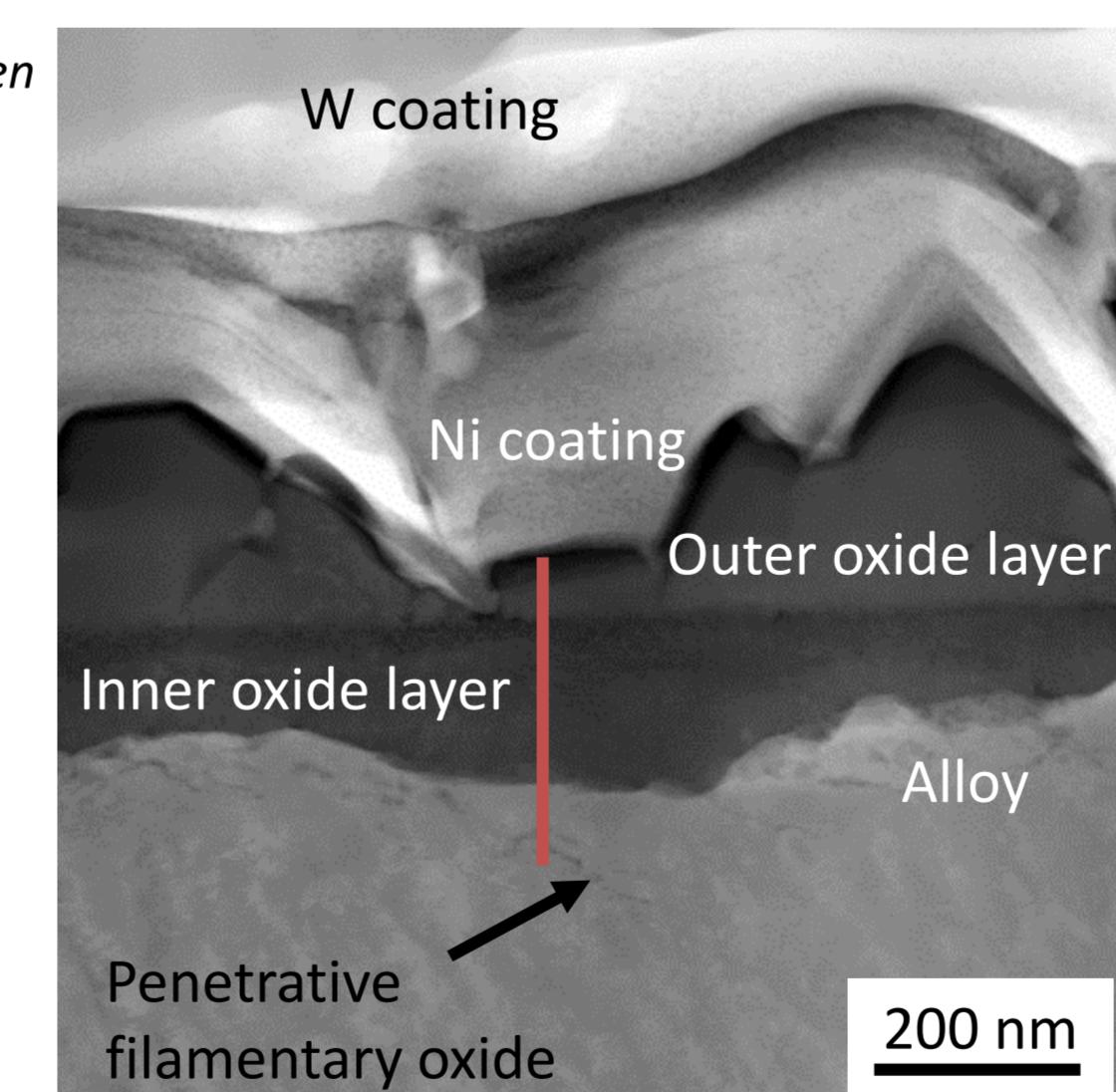
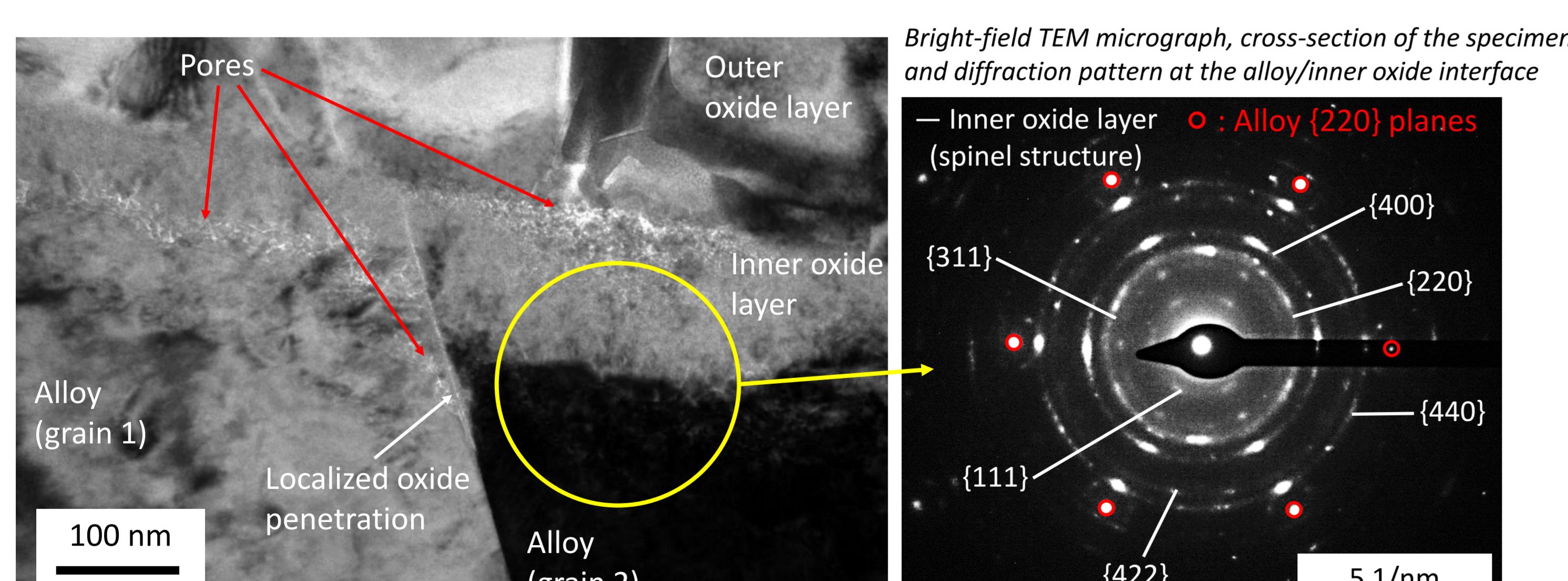


Oxidation kinetics

Specimen	Mean oxide thickness (nm)	Mean localized penetration depth (nm)
500 h	140 ± 41	92 ± 78
11% - 500 h	89 ± 43	87 ± 64
1000 h	146 ± 42	105 ± 74



TEM characterization of a non cold-worked specimen oxidized 500h at 340° C



Conclusions

SEM observations after oxidation tests in nominal PWR primary water

- Duplex surface oxide layer
- Localized oxide penetrations at grain boundaries or at slip bands
- Cold-working → lower mean oxide thickness
- Increasing oxidation times → increase of the deepest localized penetration density

Next steps

- Tests in nominal PWR primary water: oxidation kinetics and impact of cold-working on oxidation
- Adjustment of the experimental methodology for tests in aerated PWR primary water
- Tests in aerated PWR primary water → effect of dissolved O₂

TEM characterization of a non cold-worked specimen oxidized 500h at 340°C

- Inner oxide layer: randomly-oriented nano-grains of spinel structure, composition close to (Fe,Ni)(Fe,Cr)₂O₄
- Outer oxide layer: Fe-rich, possibly magnetite Fe₃O₄ (to be confirmed)