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Channel estimation strategy for LPWA transmission at low SNR: application to Turbo-FSK

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Abstract—Turbo Frequency Shift Keying has been considered as a promising physical layer for low power wide-area network connectivity. Because of its constant envelope amplitude and the efficiency of its iterative receiver performance close to Shannon’s limit can be achieved. However, results published so far in the literature for the waveform have assumed perfect channel estimation or Signal-to-noise (SNR) levels that are higher than the SNR levels considered for these applications. This paper analyzes a channel estimation strategy based on a specifically adapted pilot sequence. Simulations have been performed to evaluate the performance of the proposed approach. Performance loss induced by imperfect channel estimation algorithms is estimated.

Keywords—LPWA; Zadoff-Chu; Constant Envelope; NB-IoT

I. INTRODUCTION

The installed base of the Internet of Things (IoT) devices is forecast to grow to almost 31 billion worldwide by 2020. Long-range, wide-area networks (LPWA) including narrowband IoT (NB-IoT) are expected to make a significant part of the almost 2.6 billion Machine-to-Machine (M2M) connections that will be in place by that time [1].

For LPWA systems, low energy consumption requirement directly results from the necessity to have a long battery life. Long range is achieved with performance at a very low level of sensitivity at the receiver and obtained by ensuring Quality of Service (QoS) for low levels of Signal-to-Noise Ratio (SNR). At the physical layer, this is achieved by selecting an energy efficient modulation combined with an efficient usage of the Power Amplifier (PA), the most power-consuming component of the transmission chain [2]. The efficiency of the PA is highly dependent on the peak-to-average power ratio (PAPR) of the signal [3]. NB-IoT as defined in Release 13 of the 3GPP specification [4] considers both Single Carrier Frequency Division Multiplexing (SC-FDM) and single-tone transmission to limit peak-to-average power ratio (PAPR). The use of single tone transmission is particularly interesting for LPWA communications. Beside, this is not without any drawback. As the bandwidth is small, the transmission time duration is significantly increased in comparison to SC-FDM transmission and hence the energy to transmit an information bit. However, PAPR levels of SC-FDM is significantly larger than 0dB. For these reasons, alternatives to SC-FDM should be considered.

Turbo Frequency-Shift Keying (Turbo-FSK) is a new waveform introduced in [5] that combines a non-linear modulation with a convolutional code. Its receiver relies on turbo processing to meet a performance close to Shannon’s limit for low spectral efficiency. Furthermore, the waveform exhibits a constant envelope (i.e.: its PAPR is equal to 0 dB). Turbo-FSK

is therefore well adapted to future LPWA systems notably for the 5th generation of cellular systems.

The principles of Turbo-FSK have been first described in [5]. The motivation for the scheme was to operate close to the Shannon capacity while using a constant envelop modulation. The structure of the transmitter (Fig. 1) is composed of λ repetition stages. For each stage, a differently interleaved version of the same input information bit sequence is encoded using a simple parity accumulator. The coded bits are then mapped onto a Turbo-FSK codeword: a combination of a linear N_L -point phase shift keying (PSK) modulation and a non-linear N_{\perp} -carrier FSK modulation [6]. Efficient digital implementation can be realized by inverse Fast Fourier Transform (FFT) followed by a cyclic prefix insertion as for Orthogonal Frequency Division Multiplexing (Fig. 1). At the receiver, a soft FSK-detector estimates the probabilities of each possible Turbo-FSK codeword. These probabilities are then fed to the decoder, which uses them as channel observation, while output of the other decoders will be used as a priori information. A modified version of the algorithm proposed by Bahl, Cocke, Jelinek and Raviv (BCJR) [7] is used to decode the trellis, and derive the a posteriori probabilities of the information bits. The association of the encoding with a non-linear modulation (FSK) allows to operate at very low levels of SNR. It has been demonstrated that the choice of the PSK is the optimal modulation minimizing channel capacity gap to Shannon’s limit [8]. Practical implementations of the FSK-detector consist of a FFT combined with a frequency domain equalizer that relies on accurate channel estimation.

Expected SNR at the receiver should be well below 0dB and particularly since Turbo-FSK proposes to improve energy efficiency to within a few decibels of Shannon’s limit, . A typical level of SNR at sensitivity limit is expected to be of around -10 dB for LPWA applications. This imposes significant performance constraints on channel estimation at the receiver. Results published so far in the literature for the waveform have either assumed perfect synchronization and channel estimation or considered significantly higher levels of SNR [9]. This paper derives a channel estimation algorithm optimized for the very low levels of SNR required by low power IoT connectivity applications.

The paper is structured as follows: Section II presents a frame and pilot structure adapted to Turbo-FSK. In Section III, channel estimation algorithms are described and evaluated. Performance comparison against perfect channel estimation is given and an optimized structure is discussed. Section V concludes the paper.

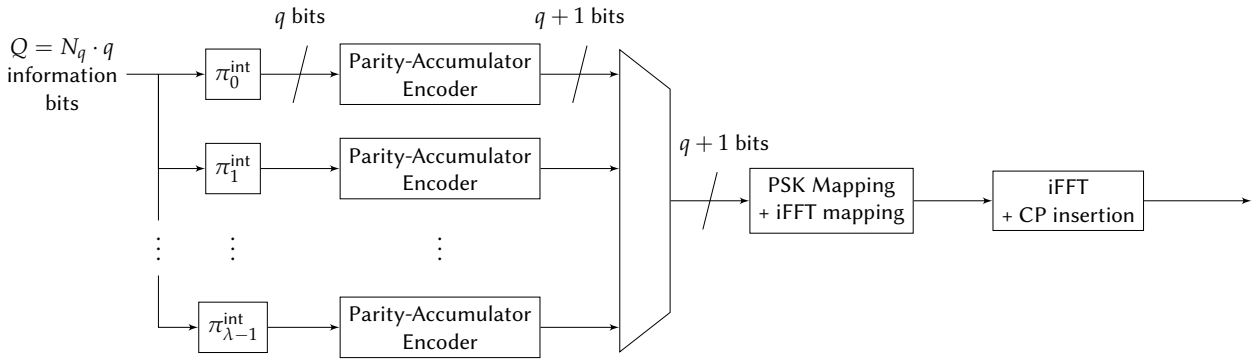


Fig. 1. Transmitter architecture of Turbo-FSK.

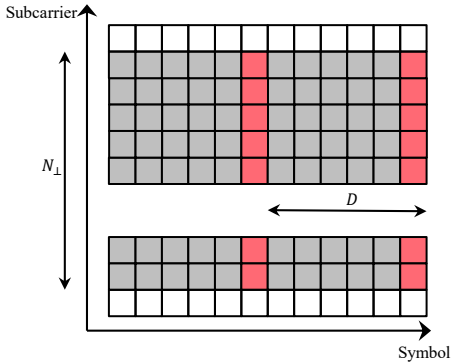


Fig. 2. Pilot structure of the frame

II. SYSTEM MODEL

A. Frame and Pilot Structure

A typical LTE uplink frame structure is considered for channel estimation. The resource grid structure where N_{\perp} subcarriers are active is composed of data symbols interleaved with pilot symbols spaced every D symbols (Fig. 2). The structure is designed to give an estimate of the frequency response of the channel and to track its evolution during the duration of the transmission. In order to keep the low-power advantage of the waveform, we imposed for the pilot symbol to have a low PAPR. As a consequence, constant amplitude, zero autocorrelation (CAZAC) sequences have been considered. Zadoff-Chu (ZC) sequences [10] are an example of such sequences and have already been widely used in cellular systems. Two approaches may be considered. For the first approach, the ZC sequence is generated in the time domain.

$$z[k] = \alpha e^{-j\pi \frac{k^2 N_{\perp}}{N^2}} e^{j2\pi\nu \frac{k}{N}}, \forall k \in [0, N] \quad (1)$$

where α is a scrambling factor that is constant for each pilot symbol, i.e. $\alpha \in \{-1, 1\}$. The parameter N_{\perp} is the number of active carriers and N the number of samples per symbol (the size of the FFT). The scalar ν is a normalized frequency offset used to shift the spectrum of the time sequence around the appropriate frequency resource block. A second approach considers the generation of the ZC sequences in the frequency domain as follows:

$$Z[k] = \alpha e^{-j\pi \frac{k^2}{N_{\perp}}}, \forall k \in [0, N_{\perp} - 1] \quad (2)$$

TABLE I. ZC SEQUENCE COMPARISON WHEN $N = 512$ AND $N_{\perp} = 32$

	PAPR [dB]	Adj. Leakage ($N_{\perp} + 1$) [dB]	Adj. Leakage ($N_{\perp} + 2$) [dB]
ZC sequence (z)	0	17.3	40.8
ZC sequence (Z)	2.6	<65.0	<65.0
Modified ZC sequence (Z), $\rho_{dB} = 7$	0.7	<65.0	<65.0

The ZC sequence of (2) is then placed on the allocated resource carriers and the associated time sequence is generated using a N -point inverse FFT. Both alternatives have advantages and drawbacks. The ZC sequence based on (1), also called time ZC sequence, provides a constant envelop signal but localization in the frequency domain is not optimal: frequency orthogonality is not ensured between synchronized users at least a guard interval of one frequency tone should be considered. For instant, up to 17.3 dB of energy is leaked to the out-of-band adjacent carrier (carrier $N_{\perp} + 1$). On the other hand, the ZC sequence based on (2), also called frequency ZC sequence, is by construction orthogonal between different users using different resource blocks, however when upsampled by the inverse FFT transform, the PAPR of the generated sequence is significantly larger than 0dB. Table I gives a performance comparison of both sequences in terms of PAPR and adjacent channel orthogonality for $N_{\perp} = 32$ and $N = 512$ where adjacent channel power leaked on carriers $N_{\perp} + 1$ and $N_{\perp} + 2$ is given.

To improve the PAPR properties of the frequency ZC sequence, we designed a modified frequency ZC sequence composed of the ZC sequence of (2) and an additive noise vector X selected in such a way that the resulting PAPR of the transmitted sequence is minimized and the signal-to-interference ratio (SIR) on each subcarrier is contained.

$$Z_{Mod}[k] = Z[k] + X[k], \text{ with } \frac{1}{|X[k]|^2} > \rho, \quad (3)$$

$\forall k \in [0, N_{\perp} - 1]$. The resulting PAPR and leakage performance of the modified ZC frequency sequence is given in Table I. Significant reduction of PAPR level is achieved: optimization gives a PAPR as low as 0.7dB when the allowed signal-to-interference level is set to 7dB.

In order to evaluate the impact on the autocorrelation properties of the ZC sequence performance, the ambiguity function of the modified frequency ZC sequence has been evaluated and

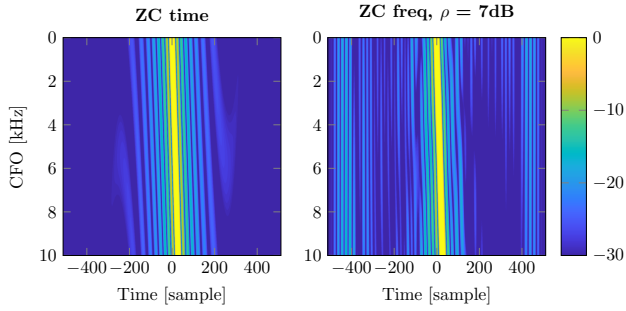


Fig. 3. Ambiguity function comparison. Left time ZC sequence as in (1) and right modified ZC frequency sequence as defined in (3)

compared to the time ZC sequence. The ambiguity function is defined as follows:

$$\mathcal{A}(f, t) = \left\| \sum_k z^*[k-t]z[k]e^{j2\pi ft} \right\|^2 \quad (4)$$

Fig. 3 gives the ambiguity function for the modified ZC sequence when ρ is set to 7dB and compared to the time sequence. It demonstrates that the interference introduced to optimize PAPR has very little impact on the autocorrelation properties of the scheme and therefore has little impact on channel estimation performance.

B. Channel Estimation

The proposed pilot sequence is used to estimate the channel information state. A three step procedure is here considered. First, a least square (LS) estimation on the pilot subcarriers is performed. Then, a de-noising filter is applied on the N_\perp LS estimates. Finally, channel estimation on pilot symbols is interpolated in the time domain to provide a channel estimate of each Turbo-FSK symbol over the duration of the transmission time interval. If \mathbf{Y} (i.e.: $Y[k], \forall k \in [0, N_\perp - 1]$) is the multicarrier symbol at the receiver after FFT associated to the transmitted pilot symbol \mathbf{Z} . Then in presence of a frequency domain complex channel \mathbf{H} and frequency domain additive white Gaussian noise, \mathbf{N} :

$$\mathbf{Y} = \mathbf{Z}\mathbf{H} + \mathbf{N} \quad (5)$$

where \mathbf{Z} is the the ZC sequence and \mathbf{N} is an additive white Gaussian noise. The least square estimate of the channel $\hat{\mathbf{H}}$ is given by:

$$\hat{\mathbf{H}} = \mathbf{H} + (\mathbf{Z}^H\mathbf{Z})^{-1}\mathbf{Z}^H\mathbf{N} \quad (6)$$

where operator H is the hermitian transpose. We will note $\tilde{\mathbf{N}}$ the white Gaussian noise colored by the ZC sequence, \mathbf{Z} :

$$\tilde{\mathbf{N}} = (\mathbf{Z}^H\mathbf{Z})^{-1}\mathbf{Z}^H\mathbf{N} \quad (7)$$

Improved estimation of the channel coefficients $\mathbf{H}[f]$ may be derived from the observation of $\hat{\mathbf{H}}[f]$ using a filter W_f designed to reject $\tilde{\mathbf{Z}}$. To construct the filter \mathbf{W}_f , the following minimization problem should be solved:

$$\arg \min_{\mathbf{W}_f} E \left[\left\| \mathbf{W}_f\hat{\mathbf{H}} - \mathbf{H} \right\|^2 \right] \quad (8)$$

Let Ω be defined as:

$$\Omega = E \left[\left\| \mathbf{W}_f\hat{\mathbf{H}} - \mathbf{H} \right\|^2 \right] \quad (9)$$

Using (6) and (7), (9) may then be rewritten as:

$$\begin{aligned} \Omega &= E \left[\left\| \mathbf{W}_f(\mathbf{H} + \tilde{\mathbf{N}}) - \mathbf{H} \right\|^2 \right] \\ &= E \left[\text{tr} \left[\mathbf{W}_f\mathbf{H}\mathbf{H}^H\mathbf{W}_f^H \right. \right. \\ &\quad \left. \left. - \mathbf{W}_f\mathbf{H}\mathbf{H}^H - \mathbf{H}\mathbf{H}^H\mathbf{W}_f^H \right. \right. \\ &\quad \left. \left. + \mathbf{H}\mathbf{H}^H + \mathbf{W}_f\tilde{\mathbf{N}}\tilde{\mathbf{N}}^H\mathbf{W}_f^H \right] \right] \end{aligned} \quad (10)$$

Then, if \mathbf{h} is the $N \times 1$ vector of the channel impulse response, \mathbf{H} may be written as:

$$\mathbf{H} = \mathbf{F}(1 : N_\perp, :) \mathbf{h} = \mathbf{F}_{N_\perp} \mathbf{h} \quad (11)$$

Finally (9) may be rewritten as:

$$\begin{aligned} \Omega &= \text{tr} \left[\mathbf{W}_f\mathbf{F}_{N_\perp} \Phi_{\mathbf{h}}\mathbf{F}_{N_\perp}^H\mathbf{W}_f^H - \mathbf{W}_f\mathbf{F}_{N_\perp} \Phi_{\mathbf{h}}\mathbf{F}_{N_\perp}^H \right. \\ &\quad \left. - \mathbf{F}_{N_\perp} \Phi_{\mathbf{h}}\mathbf{F}_{N_\perp}^H\mathbf{W}_f^H + \mathbf{F}_{N_\perp} \Phi_{\mathbf{h}}\mathbf{F}_{N_\perp}^H \right. \\ &\quad \left. + \mathbf{W}_f\mathbf{R}_{\tilde{\mathbf{N}}}\mathbf{W}_f^H \right] \end{aligned} \quad (12)$$

where $\Phi_{\mathbf{h}}$ is the time domain channel autocorrelation matrix of size $N \times N$ and $\mathbf{R}_{\tilde{\mathbf{N}}}$ is the autocorrelation matrix of the noise colored by the pilot sequence. By taking the partial derivative of Ω with respect to \mathbf{W}_f and making it equal to zero, (12) becomes:

$$\begin{aligned} \frac{\partial \Omega}{\partial \mathbf{W}_f} &= 0 \\ 0 &= (\Delta + \mathbf{R}_{\tilde{\mathbf{N}}})\mathbf{W}_f^H - \Delta \\ \mathbf{W}_f^H &= (\Delta + \mathbf{R}_{\tilde{\mathbf{N}}})^+ \Delta \end{aligned} \quad (13)$$

where $\Delta = \mathbf{F}_{N_\perp} \Phi_{\mathbf{h}}\mathbf{F}_{N_\perp}^H$. When pilots with constant amplitude are sent then the noise distribution after LS estimation is the same for each sample and therefore $\mathbf{R}_{\tilde{\mathbf{N}}} = \sigma_n^2\mathbf{I}$ with σ_n^2 the variance of the noise. However, if a modified frequency ZC sequence (as defined in (3)) are transmitted, then the amplitude of each pilot differs from one to another. Consequently the statistic of the noise after LS estimation varies and in that case, $\mathbf{R}_{\tilde{\mathbf{N}}} = \sigma_n^2\mathbf{R}_{\mathbf{NZ}}$ where $\mathbf{R}_{\mathbf{NZ}}(i, j) = 0$ when $i \neq j$, $\|\mathbf{Z}(i) + \mathbf{X}(i)\|^{-2}$ otherwise.

The question, then, is how the performance of the filter is impacted by the introduction of the interference added to limit PAPR in the case of the modified ZC sequence. Therefore performance of the proposed channel estimation scheme has been evaluated and compared to the performance of the time ZC sequence. Results of the comparison are given in the next section.

III. ESTIMATED PERFORMANCE

A. Channel estimation performance

The performance of the proposed filtered Least Square algorithm has been evaluated for both ZC sequences of (1) and (3). The size of the FFT, N , has been assumed to be equal to 512 points and N_\perp is set to 32. The relative mean square error (RMSE) of the estimated channel coefficients is evaluated for various values of SNR assuming perfect knowledge of the channel statistics (i.e. $\Phi_{\mathbf{h}}$). Results show almost identical

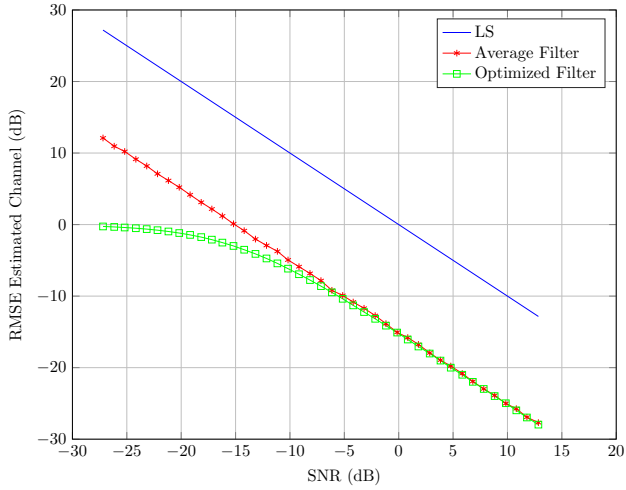


Fig. 4. Performance of channel estimation under AWGN channel.

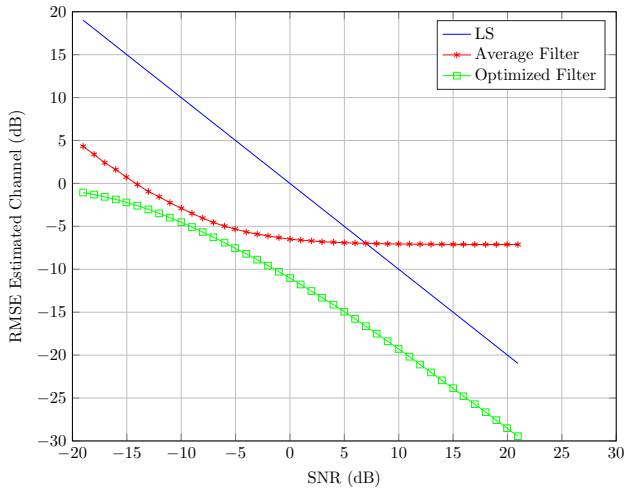


Fig. 5. Performance of channel estimation under ETU channel.

performance level between time ZC sequence and modified frequency ZC sequence. Fig. 4 gives the performance of the channel estimation method in presence of AWGN channel. The performance of the average filter is also given and is optimal in this case as the channel is a constant value. The gain of performance is significantly better than the LS approach without any filtering. In this case, an asymptotic gain of $10\log(N_{\perp})$ or 15dB is observed. The performance degradation introduced by the noise coloring of the modified frequency ZC sequence has been evaluated to be less than 0.2dB and is considered negligible.

Similarly, channel estimation performance is evaluated for the Extended Typical Urban (ETU) channel model of 3GPP. This channel emulates the impulse response of a signal received in a strong multipath environment and is typical of LPWA applications in a urban environment. In this case the coherence bandwidth is smaller than the bandwidth of the 32 active carriers (carrier spacing was 15kHz), hence the average filter is, as expected, inefficient as channel coefficients are not constant. Gain introduced by \mathbf{W}_f filter is approximately 10dB in comparison to the LS case.

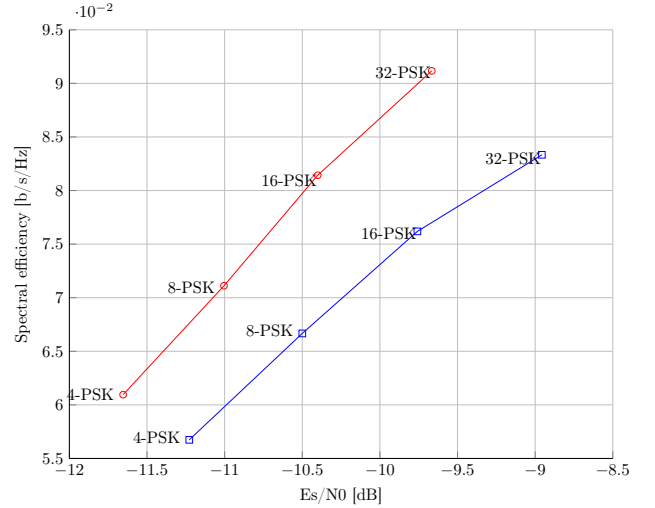


Fig. 6. AWGN performance of Turbo-FSK with $N_{\perp} = 32$ sub-carriers and N_L -PSK, $N_L = \{4, 8, 16, 32\}$, $\lambda = 4$ to reach a PER of 10^{-2} . Assuming perfect channel estimation. (red - block length equals to 1024bits - blue block length equals to 256bits)

B. Performance loss introduced by imperfect channel estimation

In order to evaluate the performance loss introduced by the proposed channel estimation scheme and the requirements put on the pilot period D as defined in Section II, performance of Turbo-FSK has been simulated under AWGN Channel (Fig. 6) for various values of N_L from 4 to 32 with $\lambda = 4$ and different payload lengths (256bits and 1024bits). This configuration has been selected as typical for LPWA applications. As expected, as the constellation order N_L is increased, spectral efficiency is also increased and the required level of SNR to reach a packet error rate (PER) less than 10^{-2} is also increased. Furthermore, SNR requirement to attain performance is lower when longer packets are transmitted. SNR interval of interest is between -12 and -9dB and well below 0dB .

Then, for the same configurations, the performance loss introduced by a non-perfect channel estimation is evaluated. AWGN is added to the perfect channel state information of the received Turbo-FSK symbols and associated performance loss as a function of the added noise on the channel state information is measured by simulation. We defined as $RMSE_H$, the amount of AWGN power that has been added. $RMSE_H$ is varied from -5dB to -20dB . Results can be found in Fig. 7 for a block length of 256-points and in Fig. 8 for a block length of 1024-points.

When $RMSE_H$ is lower than -10dB , performance loss may almost be approximated to an extra source of additive white noise. For instance, when $RMSE_H$ is equal to -10dB , performance loss introduced by an extra uncorrelated noise source should be of around $10\log(1 + 10^{-\frac{10}{10}}) = 0.4\text{dB}$. This first order approximation proves relatively correct for lower FSK constellations (4-PSK and 8-PSK). However, performance loss is significantly larger for higher values of N_L (16-PSK and 32-PSK). Furthermore, when $RMSE_H$ is larger than -10dB , significant performance degradation is observed. For data frames with a shorter payload (256bits), performance loss ranges from 1.5dB for lower values of N_L up to 3.3dB for

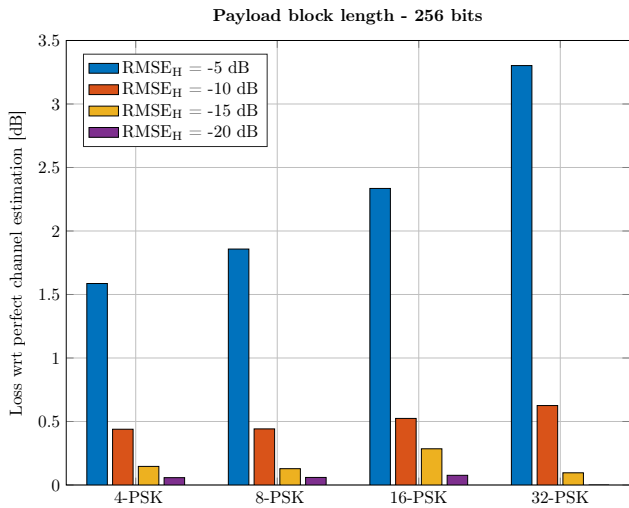


Fig. 7. Performance loss introduced by imperfect channel estimation. Payload block length 256bits.

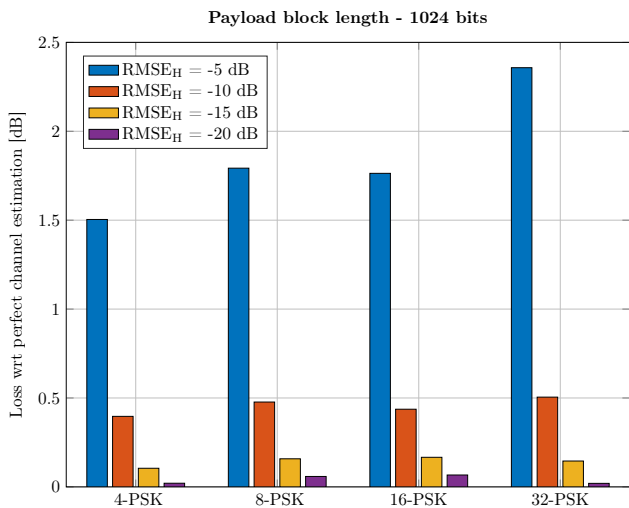


Fig. 8. Performance loss introduced by imperfect channel estimation. Payload block length 1024bits.

larger values of N_L .

C. Recommended pilot structure

These results (from Fig. 4 to Fig. 8) help derive some recommendations for channel estimation as a function of the performance loss budget allocated to channel estimation. For Turbo-FSK, performance is obtained for values of SNR between -11.5dB and -9dB . For these levels of SNR, the channel estimation of the filtered LS algorithm gives a RMSE close to -5dB when AWGN channel is considered (Fig. 4). Further noise rejection is thus necessary if performance loss incurred by channel estimation need to be contained below 1.5dB (Fig. 7 and Fig. 8). This can be achieved by interpolating the resulting channel estimation across multiple pilot symbols (time domain interpolation). Hence, channel time interpolation should not only estimate channel variations between pilot symbols but also filter unwanted noise introduced by imperfect channel estimation. To obtain $RMSE_H$ levels of -10dB (resp. -15dB) interpolation over at least 3 pilot symbols

(resp. 4) should be performed to avoid significant performance degradation.

IV. CONCLUSION

Turbo-FSK is a waveform that is well adapted to future LPWA systems for 5G systems: its performance is very close to Shannons limit and furthermore the waveform exhibits a constant envelope. However, the impact of channel estimation has so far not been thoroughly considered on the performance of the turbo-FSK receiver.

This paper discussed and evaluated a channel estimation technique based on distributed pilot symbols. A pilot sequence based on a frequency domain ZC sequence has been studied and optimized for PAPR reduction. The PAPR of the pilot sequence has been reduced to below 1dB and the performance of channel estimation has been studied. Impact on overall performance of the receiver has been evaluated particularly for the very low levels of SNR that characterize the selected LPWA scenario.

V. ACKNOWLEDGMENT

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