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New standards of absorbed dose to water under reference conditions by graphite calorimetry for $^{60}$Co and high-energy x-rays at LNE-LNHB

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Abstract
The LNE-LNHB has developed two primary standards to determine the absorbed dose to water under reference conditions (for $10 \, \text{cm} \times 10 \, \text{cm}$) in $^{60}$Co, 6 MV, 12 MV and 20 MV photon beams: a new graphite calorimeter and a water calorimeter. This first paper presents the results obtained with the graphite calorimeter and the new associated methodology. The associated relative standard uncertainty ($k = 1$) of absorbed dose to water is 0.25% for $^{60}$Co and lies between 0.32% to 0.35% for MV x-ray beams.

Keywords: absorbed dose to water, graphite calorimetry, high-energy x-rays, PENELOPE, EGSnrc, cobalt-60

(Some figures may appear in colour only in the online journal)

1. Introduction
Calorimetry is used by several National Metrology Institutes (NMIs) and the Bureau International des Poids et Mesures (BIPM) for realizing absorbed dose to water standards. A recent review of the different methods to measure photon absorbed dose can be found in the literature [1]. Some of the NMIs use water calorimetry (METAS—Switzerland, NIST—USA, NRCC—Canada, PTB—Germany, VSL—Netherlands [2–10]) and others use graphite calorimetry (BIPM, ARPANSA—Australia, BEV—Austria, ENEA-INMRI—Italy, NMIJ—Japan, NPL—United Kingdom, VNIIFTRI—Russia [11–24]).

At the LNE-LNHB, the previous absorbed dose to water references were based on the graphite calorimeter GR-8 [25] built in 1984. For a $^{60}$Co beam, the absorbed dose to graphite in a homogeneous graphite phantom (30 cm $\times$ 30 cm $\times$ 20 cm) at a depth of 5 g cm$^{-2}$ was determined from the calorimetric measurements [26, 27]. The absorbed dose to water was derived from the absorbed dose to graphite using transfer dosimeters (ionization chambers and Fricke dosimeters) placed successively in the graphite and water phantoms [28, 29]. The absorbed dose to water for the linac beams was derived from the absorbed dose to water of the $^{60}$Co beam using ionization chambers and Fricke dosimeters as transfer instruments placed successively in the $^{60}$Co and the linac beams in the water phantoms, with an energy dependence taken from the literature [30]. The corresponding relative uncertainty ($k = 1$) was 0.35% for the $^{60}$Co absorbed dose to water rate and was between 0.94% and 1.01% for the calibration coefficient of the reference ionization chamber of the linac beams. In recent years the LNE-LNHB has built new calorimeters: the graphite calorimeter GR-9 (figure 1) [31, 32] in 2006 and a water calorimeter [33]. This paper describes the results obtained with the new graphite calorimeter and the new associated methodology.

2. Absorbed dose to water in a $^{60}$Co beam
The reference point for measurements is situated at 1 m from the source and at 5 cm depth (front window included) along the
beam axis in a water phantom of dimensions 30 cm × 30 cm × 30 cm with a 4 mm front window of polymethyl methacrylate (PMMA). The beam has a diameter of 16 cm (full width at half maximum) at the reference plane.

The methodology to derive the absorbed dose to water from graphite calorimetry measurements has been streamlined in order to reduce the uncertainties and is now based on the mean absorbed dose in the graphite core and Monte Carlo calculations to convert it into absorbed dose to water (no transfer instruments involved).

2.1. Methodology

The method and the results have been presented at the ‘Conference on Advanced Metrology for Cancer Therapy’ in Braunschweig (29 November 2011) [34]. The ARPANSA has independently developed a very similar method at the same time [23]. The absorbed dose rate to water at the reference point (C) is calculated by using equation (1).

\[
\frac{\hat{D}_w(C)}{D_{\text{core}}(V)} = \frac{D_{\text{core}}(V)}{D_{\text{core}}(V)} k_{\text{MC}} k_{\text{prof}}(V) = \frac{D_{\text{core}}(V)}{D_{\text{core}}(V)} k_{\text{MC}} k_{\text{prof}}(V)
\]

where \(\hat{D}_w\) means absorbed dose rate and \(D_{\text{core}}\) the absorbed dose to water. The mean absorbed dose in the core (\(D_{\text{core}}\)) is the quantity measured within the core of the graphite calorimeter GR-9. To simplify the evaluation of uncertainties and avoid unnecessary steps, the mean absorbed dose in the core is used instead of the absorbed dose to graphite at a reference point in a homogeneous graphite phantom at a depth of 5 g cm\(^{-2}\). The ratio of the absorbed dose to water in a volume \(V\) surrounding the reference point C, \(D_{\text{core}}(V)\), to the mean absorbed dose in the core is calculated with Monte Carlo codes. The subscript MC indicates values calculated by Monte Carlo. The correction factor \(k_{\text{MC}}\) corresponds to the correction factor for the graphite-core impurities, which are too small to be included in the Monte Carlo simulations (thermists, conducting wires, silk threads,…), and \(k_{\text{prof}}(V)\) to the profile correction factor needed to convert \(D_{\text{core}}(V)\) calculated in the finite water volume \(V\) at the reference depth (5 cm for the \(\text{^{60}Co}\) beam) to \(D_{\text{core}}(C)\) at the reference point.

2.2. Graphite calorimetry

The mean absorbed dose in the core (\(D_{\text{core}}\)) is measured within the core of the graphite calorimeter GR-9 inside a graphite phantom of 30 cm × 30 cm × 20 cm (20 cm depth). The depth of the core centre is situated at 4.404 g cm\(^{-2}\).

The calorimeter consists of three concentric bodies (core, jacket, shield), inside the phantom, all made of graphite. These bodies are separated from each other by 1 mm vacuum gaps in order to provide good thermal insulation. The core, the sensitive element, is a flat cylinder of 3 mm thickness and 16 mm diameter. The jacket and the shield thicknesses are 2 mm. These different bodies are suspended by means of three silk threads taut in the median plane of the core. A lateral view of the GR-9 graphite calorimeter is given in figure 2. The radiographs of the three central bodies (front and side views) are given in figure 3.

Six negative temperature coefficient (NTC) thermistors are embedded in the core for the measurements, the thermal control and the electrical calibration. They are in the form of glass-coated beads of 0.35 mm diameter.

The components of the GR-9 core and their respective masses are given in table 1.

The graphite calorimeter can be operated in quasi-adiabatic mode or in constant-temperature mode as previously explained in detail [25]. In the quasi-adiabatic mode, the thermal quantity measured with one thermistor is the temperature rise in the core during the irradiation. The other thermistors are used for the electrical calibration and the thermal control. For the constant-temperature mode, the core is maintained at an assigned temperature by means of controlled and measured electrical power. During irradiation, this measured electrical power is lower because the energy imparted by the ionizing radiation in the graphite is converted into heat. The quantity of interest is the difference of electrical power when the beam is successively off and on. The statistical uncertainties are reduced with this method which is used with the new calorimeters (GR-9 and GR-10).

The earlier GR-8 graphite calorimeter, with a core of the same dimensions, and the most recent one, GR-10, of small cross section adapted for use in the small beams of Intensity-Modulated Radiation Therapy, have been successfully compared with the GR-9 calorimeter used in the present study [32, 35]. The values of absorbed dose to water in \(\text{^{60}Co}\) obtained by measurements with the GR-9 and GR-10 calorimeters differed by less than 0.1% with a combined standard uncertainty of 0.3% on their ratio and the GR-8/GR-9 \(D_{\text{core}}\) ratios obtained by measurements and by Monte Carlo calculations were within 0.2% of unity, with a statistical uncertainty of 0.3% in the 6 MV and 12 MV beams.

In the present study, the measurements have been made in two campaigns and the mean value of both campaigns is used to determine the mean absorbed dose rate in the core. The type-A uncertainty of \(\hat{D}_{\text{core}}\) is equal to 0.014%.
2.3. Monte Carlo calculations

A detailed description of the calculations is presented hereafter, as the calculated dose ratio \( D_w(V)/D_{\text{core}}^{\text{MC}} \) is of critical importance in the determination of the absorbed dose to water.

Two different codes were used for the Monte Carlo simulations of the LNE-LNHB \(^{60}\)Co irradiator: EGSnrc v4-r2-3 [36–38] and PENELOPE 2006 [39].

The particles crossing a plane 10 cm ahead of the reference plane (5 cm ahead of the water phantom surface and at 90 cm from the \(^{60}\)Co source) are stored in a phase space file (PSF). The PSFs are created using both BEAMnrc (beam2008rc1) and Penmain_mpi (2.52), a parallelised version of PENELOPE 2006 [40]. As the cobalt irradiator has a cylindrical geometry, the particles are split 5 times and rotated around the beam axis. The McTwist module [41] was added into BEAMnrc to introduce this type of variance reduction technique. With the PENELOPE code, the simulation of electron transport processes is controlled by specifying values for several parameters: \( C_1 \), \( C_2 \), \( W_{\text{CC}} \) and \( W_{\text{CR}} \). \( C_1 \) and \( C_2 \) control, respectively, the average angular deflection produced by multiple elastic scattering of electrons along the step between hard events and the maximum average fractional energy loss in the step. \( W_{\text{CC}} \) and \( W_{\text{CR}} \), respectively, represent the cutoff energy loss for hard inelastic collisions and for hard bremsstrahlung emission. For the PSF creation, the
are replaced by graphite and the impurities external to the core are replaced by vacuum (thermistor wires and silk threads). The calculation is derived from general cavity theory. The Monte Carlo calculation of the photon and electron spectra allows the estimation of the mean mass energy absorption coefficients and mass stopping powers. The value of the correction factor and its uncertainty are given in table 5.

The profile correction factor in the water volume $V$ (thickness 3 mm, diameter 16 mm), $k_{\text{prof}}(V) = D_w(C)/D_w(V)$ is divided into two terms: a longitudinal one (along the beam axis) and a radial one (perpendicular to the beam axis). The beam is assumed to have cylindrical symmetry along the beam axis and around the reference point in the water volume $V$. Along the beam axis, the longitudinal correction is assumed to be equal to unity with a negligible uncertainty. The radial correction (on a disc with a diameter of 16 mm) is calculated based on the horizontal ($X$) and vertical ($Y$) profiles measured inside the water phantom with a small volume ionization chamber. The profile measurements $X$ and $Y$ are symmetrised, and a radial profile ($R$) calculated from the horizontal and vertical profiles: $R = (X + Y)/2$. The radial profile $R$ is fitted with a polynomial function $g$ (easy to integrate) and $k_{\text{prof}}(V)$ is calculated with equation (2).

$$k_{\text{prof}}(V) = \frac{R(C)}{\int_0^{r_{\text{min}}} g(r) r \, dr / \int_0^{r_{\text{max}}} r \, dr}$$

with $r_{\text{max}}$ radius of the disc and $R(C)$ value of the radial profile $R$ at the reference point C. The type-A uncertainty is calculated from the measurement reproducibility at point C. The type-B uncertainty is evaluated from the difference between the same calculations with $R$ taken equal to $X$ or to $Y$ as extreme cases, plus 0.02% due to the method. In the $^{60}$Co beam with the cylindrical symmetry, $X$ and $Y$ are very similar.

It is possible to compare the products $[D_w(V)/D_{\text{core}}]_{MC}$ for the volumes $V$ with the diameters of 1.6 cm and 2 cm. The difference is less than 3 parts in $10^4$.  

### 3. Absorbed dose to water in a linac photon beam

The method is very close to the one described in section 2 with a few notable differences. Instead of relying on irradiation time, radiation monitors are used. Instead of calculating a dose rate, a reference ionization chamber is calibrated in the water phantom. This work has been carried out in the 6 MV, 12 MV and 20 MV beams of the Saturne 43 medical linear accelerator at the LNE-LNHB laboratory. The reference point is situated at 10 cm depth (4 mm front window of PMMA within a square of 12 cm side included) along the beam axis in a water phantom of $30 \times 30 \times 30$ cm.

#### 3.1. Methodology

The calibration coefficient for absorbed dose to water at the reference point ($N_{Dw}$) is calculated using equation (3):

$$N_{Dw} = \frac{D_w(C)/D_{\text{core}}}{Q_w/ma} = \frac{D_w(C)/D_{\text{core}}}{Q_w/ma} \left[ \frac{D_w(V)}{D_{\text{core}}(V)} \right]_{MC} k_{\text{prof}}(V)$$  

### 2.4. Correction factors

The impurity correction factor $k_i$ takes into account all the details in the core that are not included in the simulation (for example thermistors, silk wires and resin). They are determined by considering that the impurities within the core have identical to those described for the LNE-LNHB high-energy parameters specific to each Monte Carlo code are taken as default values [42] in both codes. The values of other water were taken as equal to 78 eV and 75.0 eV respectively.  

### Table 2. Cutoff energies for the PSF creation.

<table>
<thead>
<tr>
<th>$E_{\text{cut}}$/keV</th>
<th>Photons</th>
<th>Electrons$^a$</th>
<th>Electrons$^a$</th>
</tr>
</thead>
<tbody>
<tr>
<td>EGSnrc</td>
<td>10</td>
<td>89</td>
<td>89</td>
</tr>
<tr>
<td>PENELOE</td>
<td>10</td>
<td>100</td>
<td>200</td>
</tr>
</tbody>
</table>

$a$ Kinetic energy cutoff.

### Table 3. Cutoff energies for the dose calculations.

<table>
<thead>
<tr>
<th>$E_{\text{cut}}$/keV</th>
<th>Photons</th>
<th>Electrons$^a$</th>
</tr>
</thead>
<tbody>
<tr>
<td>EGSnrc</td>
<td>10</td>
<td>10</td>
</tr>
<tr>
<td>PENELOE</td>
<td>5</td>
<td>50</td>
</tr>
</tbody>
</table>

$a$ Kinetic-energy cutoff.

Penelope values used are $C_1 = C_2 = 0.10$. The parameter values $W_{\text{CC}}$ and $W_{\text{CR}}$ are set equal to the values presented in table 2. The cutoff energies of both codes are summarized in table 2. Each PSF created contains around $4.5 \times 10^8$ particles.

The PSFs are used to calculate $D_w(V)$ and $D_{\text{core}}$. The particles in the PSF are split 24 times with EGSnrc (NRCYCL parameter in the DOSRZnrc program) and 25 times with Penmain mpi. The cutoff energies are summarized in table 3. The mean excitation energies of graphite (calorimeter) and water were taken as equal to 78 eV and 75.0 eV respectively (default values) [42] in both codes. The values of other parameters specific to each Monte Carlo code are taken as identical to those described for the LNE-LNHB high-energy x-ray beams study (see section 3.3).

The volume of water $V$ centred on the reference point C has a cylindrical shape with its revolution axis identical to the beam axis. The cylinder diameter is 16 mm and its thickness is 3 mm (identical to the calorimeter core). The water phantom PMMA walls have a thickness of 15 mm except on the beam axis where the thickness is only 4 mm within a diameter of 12 cm.

The results of the calculations of $[D_w(V)/D_{\text{core}}]_{MC}$ are summarized in table 4. The uncertainties (in parentheses) correspond only to type-A uncertainties ($k = 1$) from the calculations. The two code results are in agreement to better than 0.1%. The weighted mean of both code results is chosen for the calculations of the absorbed dose to water. The type-A relative uncertainty for the weighted mean is conservatively taken equal to the largest uncertainty value obtained with the standard deviation of the sample or with the standard deviation of a weighted mean. The type-B relative uncertainty on the dose ratio is evaluated to be 0.2% based on comparisons between calculated and measured dose ratios [43].

Calculations have also been done for a cylindrical volume of water $V$ with a diameter of 2 cm instead of 1.6 cm. The ratio between the two code results is then 1.0007 instead of 1.0006.

#### 2.4. Correction factors

The impurity correction factor $k_i$ takes into account all the details in the core that are not included in the simulation (for example thermistors, silk wires and resin). They are determined by considering that the impurities within the core...
D is made with one phantom close to the other. To ensure that equations below, the notation ‘ means that the measurement measurement results should be linked to the charge of the reference ionization chamber in water as directly as possible. To do this, a device was built with the water and graphite phantoms both placed on a mobile tray that can be easily moved to put one phantom in front of the beam and the other out alternately (figure 4). In this way, it was possible to make measurements in the water phantom with the reference ionization chamber in the morning and the evening, before and after the calorimetric measurements.

To check that the monitor information when the water phantom is irradiated, is equivalent to the monitor information when the graphite phantom is irradiated (possible differences in backscattered radiation from the phantoms), measurements were made consecutively with ionization chambers in the water \( Q_w \) and the graphite \( Q_c \). The ratio between these charges per monitor unit \( \frac{Q_w \mu}{Q_c \mu} \) has been examined using different monitors. The preferred monitor is placed at the linac head exit, just outside the direct beam. This external additional monitor is more reliable than the internal one supplied with the linac. However, this internal monitor is located well inside the head so it has less dependence on the backscatter of the phantoms. If there is a difference in backscatter on the external monitor due to phantom differences, the charge ratio will be different when normalized to the internal or to the external monitor. The maximum observed discrepancy was of the order of 1 part in \( 10^4 \), which is well within the statistical uncertainties (4 to 7 parts in \( 10^3 \)).

Another point to be checked was whether locating one phantom close to the other contributes to the detection of more scattered radiation in the irradiated phantom. In the equations below, the notation ‘ means that the measurement is made with one phantom close to the other. To ensure that \( \frac{Q_{\text{core}/\mu}}{Q_w \mu} = \frac{Q_{\text{core}/\mu}}{Q_w \mu} \mu /Q_w \mu \) or \( \frac{Q_{\text{core}/\mu}}{Q_w \mu} = \frac{Q_{\text{core}/\mu}}{Q_w \mu} \mu /Q_w \mu \), measurements with ionization chambers were made in the water phantom \( Q_w \mu \) and in the graphite phantom \( Q_c \mu \) with and without the other phantom by their side. The charge ratios in table 6 should be larger than one if the effect is significant. At 6 MV where the scattering should be the largest of the three beams, the measured effect was less than \( 3 \times 10^{-4} \), well within the corresponding statistical uncertainty of \( 5.3 \times 10^{-4} \).

Simulations have been done with EGSnrc to evaluate the effect of the additional phantom on the term \( \frac{D_w \mu (V)}{D_{\text{core}/\mu}} \). The calculated effect was less than 5 parts in \( 10^5 \) for the 6 MV beam and less than 1 part in \( 10^4 \) for the 20 MV beam, well within the relative statistical uncertainties of \( 27 \times 10^{-4} \) and \( 12 \times 10^{-4} \) respectively.

### Table 4. Calculated ratio \( \frac{D_w \mu (V)}{D_{\text{core}/\mu}} \) for \( ^{60}\text{Co} \).

<table>
<thead>
<tr>
<th>PENEOLE</th>
<th>EGSsrc</th>
<th>PENEOLE/EGSsrc</th>
<th>Weighted mean</th>
<th>Type A/10^2</th>
<th>Type B/10^2</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.0414 (12)</td>
<td>1.0408 (18)</td>
<td>1.0006 (20)</td>
<td>1.0412</td>
<td>0.094</td>
<td>0.2</td>
</tr>
</tbody>
</table>

* Relative standard uncertainties.

### Table 5. Correction factors and standard uncertainties.

<table>
<thead>
<tr>
<th>( k_i )</th>
<th>( \frac{k_{\text{test}} (V)}{Q_w \mu} )</th>
<th>( \frac{k_{\text{test}} (V)}{Q_c \mu} )</th>
<th>( \frac{k_{\text{test}} (V)}{Q_w \mu} )</th>
<th>( \frac{k_{\text{test}} (V)}{Q_c \mu} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.9992</td>
<td>1.0002</td>
<td>0.01</td>
<td>0.02</td>
<td></td>
</tr>
</tbody>
</table>

* Relative standard uncertainties.

where ‘/\( \mu \)’ in the subscript means that the quantity is /\( \mu \) per monitor unit. \( Q_w \) is the charge measured by the reference ionization chamber in the water phantom corrected for temperature, pressure and humidity. \( Q_c \mu \) is the charge \( Q_w \) corrected for polarity, recombination and radial anisotropy.

As can be seen in equation (3), the calorimeter \( \frac{Q_w \mu}{Q_c \mu} \) with their statistical uncertainties.

**3.2. Graphite calorimetry measurements**

The absorbed dose in the core \( D_{\text{core}/\mu} \) is measured within the core of the graphite calorimeter GR-9 inside a graphite phantom of 30 cm × 30 cm × 20 cm. The depth of the core centre is situated at 9.379 g cm\(^{-2}\).

One day of measurements of \( \frac{D_{\text{core}/\mu}}{Q_w \mu} \) (graphite calorimetric measurements bracketed by the ionization chamber measurements in the morning and evening) is considered as a single measurement for the calculation of uncertainties. The type-B uncertainties in table 7 correspond to the uncertainties on the monitor unit measurement (/\( \mu \)) and \( Q_w \).
3.3. Monte Carlo calculations

A detailed description of the calculations is presented hereafter, as the calculated dose ratio \( D_{\text{MC}}(V)/D_{\text{core}} \) is of critical importance in the determination of the absorbed dose to water.

For each beam and detector studied, the Monte Carlo calculations are divided into two successive steps: creation of PSFs after adjustment of the initial accelerator beam parameters, and dose calculation within the specific geometry of each studied detector (taking into account the volume, shape, density and composition of the various detector components).

3.3.1. Creation of PSFs at the accelerator head output. The purpose of the first step is to determine for a given beam, i.e. with a specific nominal energy and irradiation field size, the characteristics of the initial incident electrons upstream of the accelerator head. Among the various adjustable parameters available, the most important are the electron kinetic energy and the electron impact location on the titanium sheet separating the vacuum of the accelerating cavities from the ambient air in the irradiation room. The incident electron location and kinetic energy distributions are assumed to be Gaussian. In practice, a PSF with a reduced number of particles is generated and used to calculate the beam axis depth-dose distribution and the dose radial anisotropy at 10 cm depth into a 30 cm × 30 cm × 30 cm water-filled tank volume. A maximum of 3 to 4 attempts with different parameter sets (specific electron initial energy and location distributions) are performed for a given beam. The set of parameters which gives the best agreement in terms of radial anisotropy and depth-dose distribution with experimental measurements is considered to correspond to the reference initial parameters for the studied beam. This approach is used concurrently for both Monte Carlo codes used in this study. Therefore, the set of initial parameters can be slightly different from one code to another. Then one PSF of larger dimension is generated according to the initial reference parameter set. The created PSF contains between 150 × 10^6 and 800 × 10^6 particles.

Two different codes were used for the Monte Carlo calculations of the SATURNE 43 linear accelerator: EGSnrc v4-r2-2–5 [36, 38] in association with BEAMnrc (beam2007), and PENELOPE 2004 [44]. The calculations have been made on a processor cluster. To run PENELOPE on several processors without overlapping of the random number sequences, seed numbers sufficiently apart in the random sequence were chosen to begin each calculation on a different processor.

The Monte Carlo programs used in this study are shown in table 8:

### Table 7. Uncertainties of \( \frac{D_{\text{MC}}(V)}{D_{\text{core}}} \).

<table>
<thead>
<tr>
<th>Code</th>
<th>Type A/10^-2</th>
<th>Type B/10^-2</th>
</tr>
</thead>
<tbody>
<tr>
<td>6 MV (3 days)</td>
<td>0.031</td>
<td>0.17</td>
</tr>
<tr>
<td>12 MV (3 days)</td>
<td>0.028</td>
<td>0.17</td>
</tr>
<tr>
<td>20 MV (6 days)</td>
<td>0.051</td>
<td>0.13</td>
</tr>
</tbody>
</table>

* Relative standard uncertainties.

### Table 8. Monte Carlo programs.

<table>
<thead>
<tr>
<th>Code</th>
<th>PSF creation</th>
<th>Dose calculation</th>
</tr>
</thead>
<tbody>
<tr>
<td>BEAMnrc/EGSnrc</td>
<td>BEAMnrc/DOSXYZnrc</td>
<td>DOSRZnrc</td>
</tr>
<tr>
<td>PENELOPE</td>
<td>PSF/Dose3D</td>
<td>Modified/ Pendoses</td>
</tr>
</tbody>
</table>

### Table 9. Cutoff energies for the PSF creation.

<table>
<thead>
<tr>
<th>( E_{\text{cut}} ) (keV)</th>
<th>electrons in air</th>
<th>electrons not in air</th>
</tr>
</thead>
<tbody>
<tr>
<td>EGSnrc</td>
<td>10</td>
<td>189</td>
</tr>
<tr>
<td>PENELOPEb</td>
<td>20/50</td>
<td>500/1000</td>
</tr>
</tbody>
</table>

* Kinetic energy cutoff.

The DOSXYZnrc and DOSRZnrc programs are associated respectively with the BEAMnrc distribution and EGSnrc code. More complete information is available through their respective user manuals (DOSXYZnrc [45], DOSRZnrc [37]). The PSF and Dose3D programs were developed for previous calculations made at LNE-LNHB [43, 46]. The modified Pendoses program dedicated to the dose calculation corresponds to the Dose3D program except for the scoring areas. The energy depositions are not partitioned in voxels, but in the volumes of the detectors such as the core of the graphite calorimeter (diameter 16 mm, thickness 3 mm) or the water volume \( V \) around the reference point (diameter 16 mm, thickness 3 mm).

For the PSF creations, the parameters of the EGSnrc code were set to the default values except for three parameters. The pair angular distribution is based on formula 2BS of Koch and Motz [47]. The Bremsstrahlung events were simulated on the basis of the National Institute of Standards and Technology (NIST) differential Bremsstrahlung cross sections [48, 49] and the value of the maximum electron step length, SMAX, is set equal to 5 cm.

For the PSF creation, the PENELOPE values used are \( C_1 = C_2 = 0.10 \) and \( W_{\text{MC}} = 10 \text{ keV} \), \( W_{\text{CR}} = 50 \text{ keV} \). The cutoff energies of both codes are summarized in table 9.

The variance reduction techniques used with PENELOPE are those developed by Mazurier et al [50]. They artificially increase the number of created Bremsstrahlung photons and the flux of photons towards the beam aperture. The values of the parameters \( FMFP \) (forced mean free path) and \( PKILL \) (killing probability) are identical to those taken by Mazurier (\( FMFP = 0.006 \text{ cm} \) for 12 MV and 20 MV, \( 0.005 \text{ cm} \) for 6 MV, \( PKILL = 0.9 \)). The value of the parameter \( NSPLIT \) (splitting number) is set equal to 5.

The directional Bremsstrahlung splitting (DBS) is called with the BEAMnrc program. Each Bremsstrahlung photon is split into 1500 particles (parameter IBRSPL). Moreover, at the flattening filter level, the electrons are split with the same factor and redistributed with radial symmetry about the beam axis. The global cutoff energy value for electron range rejection, ESAVE, is set equal to 2 MeV.

### 3.3.2. Dose calculations.

For the dose calculations, the effects of electron impact ionization (inner shell vacancies) and...
Rayleigh scattering are taken into account in the DOSRZnrc program. The EGS value of global energy loss constraint, 

\[ \text{ESTEPE} \]

is set equal to 0.04.

The PENEOPE selected parameter values for the modified Pendoses program are \( C_1 = 0.15 \), \( C_2 = 0.10 \) and \( W_{CC} = W_{CR} = 5 \) keV. The maximum allowed step length between hard interactions of electrons and positrons, \( \text{DSMAX} \), is set to ensure that, on average, there will be more than 20 soft events along a typical electron/positron track within specific regions (i.e. the sensitive part of the detector).

The cutoff energies of both codes are the same as those used for \( { }^{60}\text{Co} \) and are summarized in table 3.

Given the square shape of the radiation beam, the effective number of particles in the PSF created by the PENEOPE code has been multiplied by a factor of 4 by considering the particle and its three symmetrical counterparts. The number \( \text{NSPLIT} \) of identical particles used with the Russian roulette method is set equal to 10.

The only variance reduction technique used by the DOSRZnrc program is to reuse each particle stored into the PSF files \( \text{NRCYCL} \) times, with \( \text{NRCYCL} \) set equal to 30.

The results of the calculations of \( [D_w(V)/D_{\text{core,MC}}]_{\text{PSF}} \) are summarized in table 10. The absolute uncertainties (in parentheses) correspond only to type-A uncertainties \( (k = 1) \). The results of the two codes agree within uncertainties, the largest observed discrepancy being 0.25%.

### 3.4. Correction factors

The impurity correction factor \( k_i \) takes into account all the details in the core that are not included in the simulation (for example thermistors, silk wires, resin). The determination of this correction factor is described in section 2.4. Its value and the associated uncertainty are given in table 11.

The profile correction factor on the water volume \( V \) of water with a diameter of 2 cm instead of 1.6 cm. Again the two codes agree within uncertainties, the largest observed discrepancy being 0.25%.

### 4. Results and discussion

#### 4.1. Absorbed dose to water with the graphite calorimeter

For the \( { }^{60}\text{Co} \) beam, the different components necessary to calculate the absorbed dose rate to water are summarized in table 13. \( k_{\text{asym}} \) corrects for the slight asymmetry when the calorimeter is irradiated from the front or from the back. This asymmetry may come from density variations in the graphite

<table>
<thead>
<tr>
<th>PENEOPE</th>
<th>EGSnrc</th>
<th>PENEOPE/EGSnrc</th>
<th>weighted mean</th>
<th>Type A$^2/10^{-2}$</th>
<th>Type B$^2/10^{-2}$</th>
</tr>
</thead>
<tbody>
<tr>
<td>6 MV</td>
<td>1.0123 (25)</td>
<td>1.0144 (14)</td>
<td>0.9979 (28)</td>
<td>1.0139</td>
<td>0.147</td>
</tr>
<tr>
<td>12 MV</td>
<td>1.0477 (21)</td>
<td>1.0484 (14)</td>
<td>0.9994 (25)</td>
<td>1.0482</td>
<td>0.114</td>
</tr>
<tr>
<td>20 MV</td>
<td>1.0631 (15)</td>
<td>1.0647 (85)</td>
<td>0.9986 (16)</td>
<td>1.0643</td>
<td>0.102</td>
</tr>
</tbody>
</table>

* Relative standard uncertainties.

<table>
<thead>
<tr>
<th>( k_i )</th>
<th>( u_i^2/10^{-2} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>6 MV</td>
<td>0.9971</td>
</tr>
<tr>
<td>12 MV</td>
<td>0.9968</td>
</tr>
<tr>
<td>20 MV</td>
<td>0.9967</td>
</tr>
</tbody>
</table>

* Relative standard uncertainties.

Calculations have also been done for a cylindrical volume \( V \) of water with a diameter of 2 cm instead of 1.6 cm. Again the two codes agree within uncertainties, the largest observed discrepancy being 0.25%.
and has been measured in the $^{60}$Co beam. $k_{gw}$ corrects the Monte Carlo calculations which have been done with a water mass density of 1 instead of 0.99823 g cm$^{-3}$ (20 °C). To correct for the decay of the source ($k_t$) between the 1 July 2004 (date close to the measurements in $^{60}$Co) and the 1 January 2002 (reference date), a half-life of 5,2711 (8) years is taken [52]. The relative uncertainty of the rate of absorbed dose to water ($k = 1$) is 0.25%. This dose rate of 56.91 (14) Gy/h is higher by 0.19% than the previous reference dose rate based on the graphite calorimeter GR-8 and an experimental graphite-to-water transfer made with Fricke dosimeters and ionization chambers. It should also be noted that the graphite phantom was not of the same density as the one used in this study (1.74 g cm$^{-3}$ previously and 1.85 g cm$^{-3}$ now).

For the linac beams, the different components necessary to calculate the absorbed dose to water calibration coefficient of the reference ionization chamber NE 2571 (# 2791) are summarized in table 14. $k_{asym}$ has been calculated based on the measurements in the $^{60}$Co beam. The thickness of the NE 2571 chamber PMMA waterproof sleeve is 0.5 mm. The LNE-LNHB $k_Q$ values corresponding to the previous methodology described in the introduction are shown in figure 6 (LNHB 1998) with crosses ‘+’ and without uncertainties for clarity as these standard uncertainties are between 0.87% and 1.1%. The new points are represented with ‘x’ uncertainties (between 0.41% and 0.44%) and are lower than the previous ones. The protocol TRS-398 [56] proposes uncertainties of 1%. The calculations of Muir and Rogers [57] with uncertainties of 0.28% (if W, mean energy expended in air per ion pair formed, is assumed constant) or 0.57% (if W is not constant) are closer to our $k_Q$ as well as the calculations of Wulff et al [58] with uncertainties between 0.3% (6 MV) and 0.5% (24 MV) [59]. The thickness of the PMMA waterproof sleeve was taken equal to 1 mm for the calculations. Compared to the experimental points [7, 60–62] all based on water calorimetry, the new $k_Q$ values obtained for the reference NE 2571 ionization chamber are in the low region. The different thicknesses of the waterproof sleeves can partly explain the $k_Q$ value differences.

### 4.3. Comparisons

The LNE-LNHB regularly participates in key comparisons of absorbed dose to water for $^{60}$Co beams with the BIPM [63]. The previous comparison occurred in April 2013 and the ratio of the absorbed dose to water of LNE-LNHB and BIPM standards was 0.9971 (39). Using only the graphite calorimeter GR-9 and assuming that nothing else changed, the ratio would have been 0.9976 (40).

The BIPM has started a comparison programme with its graphite calorimeter in high-energy photon beams [51, 64–67] of the linacs of primary standard laboratories. The comparison with LNE-LNHB at 6 MV, 12 MV and 20 MV took place in March 2012 [65]. The ratios of the absorbed dose to water of LNE-LNHB and BIPM standards were 0.9952 (44), 0.9948 (47) and 0.9938 (50) for the 6 MV, 12 MV and 20 MV beams respectively. Using only the graphite calorimeter GR-9 and assuming that nothing else changed, the ratios would have been 0.9965 (48), 0.9943 (50) and 0.9952 (52).
Table 14. \( N_{\text{Dw}}(C) \) of the reference ionization chamber (NE 2571 # 2791) based on graphite calorimetry.

<table>
<thead>
<tr>
<th></th>
<th>6 MV</th>
<th>12 MV</th>
<th>20 MV</th>
</tr>
</thead>
<tbody>
<tr>
<td>TPR(_{20,10}) without ( k_s )</td>
<td>0.676 86 (35)</td>
<td>0.749 19 (38)</td>
<td>0.783 61 (40)</td>
</tr>
<tr>
<td>TPR(_{20,10}) with ( k_s )</td>
<td>0.676 43 (38)</td>
<td>0.748 28 (41)</td>
<td>0.782 47 (42)</td>
</tr>
<tr>
<td>[ \frac{D_{\text{ref}}(C)}{D_{\text{ref}}(\gamma)} ] (Gy/C)</td>
<td>( 4.4110(75) \times 10^7 )</td>
<td>( 4.2236(70) \times 10^7 )</td>
<td>( 4.1117(57) \times 10^7 )</td>
</tr>
<tr>
<td>( k_{\text{TPR}} )</td>
<td>1.000 50 (20)</td>
<td>1.000 38 (20)</td>
<td>1.000 32 (20)</td>
</tr>
<tr>
<td>( (D_{\text{w}}(V)/D_{\text{core}})_{\text{MC}} )</td>
<td>1.0139 (25)</td>
<td>1.0482 (24)</td>
<td>1.0643 (24)</td>
</tr>
<tr>
<td>( k_{\rho W} )</td>
<td>1.00060 (2)</td>
<td>1.00045 (1)</td>
<td>1.00038 (2)</td>
</tr>
<tr>
<td>( k_{\text{prof}}(V) )</td>
<td>1.00065 (79)</td>
<td>0.99814 (82)</td>
<td>1.00351 (93)</td>
</tr>
<tr>
<td>( k_i )</td>
<td>0.9971 (10)</td>
<td>0.9968 (10)</td>
<td>0.9967 (10)</td>
</tr>
<tr>
<td>( k_{\text{pol}} )</td>
<td>0.99910 (33)</td>
<td>0.99909 (33)</td>
<td>0.99898 (33)</td>
</tr>
<tr>
<td>( k_{\text{in}} )</td>
<td>1.00282 (56)</td>
<td>1.00546 (56)</td>
<td>1.00534 (56)</td>
</tr>
<tr>
<td>( N_{\text{Dw}}(\text{Gy/C}) )</td>
<td>4.454(15) \times 10^7</td>
<td>4.395(15) \times 10^7</td>
<td>4.340(14) \times 10^7</td>
</tr>
<tr>
<td>( \mu_c(N_{\text{Dw}})/N_{\text{Dw}} / 10^{-2} )</td>
<td>0.35</td>
<td>0.33</td>
<td>0.32</td>
</tr>
</tbody>
</table>

Figure 6. Experimental and calculated \( k_Q \) values for a NE 2571 ionization chamber according to different sources.

These results are in very good agreement with those of the ARPANSA [67], which used a very similar method based on graphite calorimetry: 0.9965, 0.9924 and 0.9932 for 6 MV, 10 MV and 18 MV respectively.

Looking at figure 6 at the differences between the \( k_Q \) values for high-energy x-rays presented in this study and the experimental values obtained with water calorimetry, and looking at the good agreement between LNHB and ARPANSA via the BIPM.RI(I)-K6 comparisons, one could infer the possible existence of two different sets of results available today according to the type of calorimeter used, i.e. graphite or water. The next comparisons between the BIPM and other primary standards laboratories should confirm or refute this theory.

5. Conclusions

The LNE-LNHB has developed a new graphite calorimeter to determine the absorbed dose to water under reference conditions (10 cm × 10 cm) in \( ^{60}\text{Co} \), 6 MV, 12 MV and 20 MV high-energy photon beams. The methodology used to calculate the absorbed dose to water with the graphite calorimeter is now based on the absorbed dose in the core and Monte Carlo calculations. The relative standard uncertainty (\( k = 1 \)) is 0.25% for \( ^{60}\text{Co} \) and lies between 0.32% and 0.35% for MV x-ray beams. Another paper describing our work based on the water calorimeter will be presented in the future. The results obtained with the two methods will then be compared.
Acknowledgments

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