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## Design and acceptability assessment of a new reversible orthosis

N. Jarrassé, J. Robertson, P. Garrec, J. Paik, V. Pasqui, Y. Perrot, A. Roby-Brami, D. Wang, G. Morel

**Abstract**— We present a new device aimed at being used for upper limb rehabilitation. Our main focus was to design a robot capable of working in both the *passive mode* (i.e. the robot shall be strong enough to generate human-like movements while guiding the weak arm of a patient) and the *active mode* (i.e. the robot shall be able of following the arm without disturbing human natural motion). This greatly challenges the design, since the system shall be reversible and lightweight while providing human compatible strength, workspace and speed. The solution takes the form of an orthotic structure, which allows control of human arm redundancy contrarily to clinically available upper limb rehabilitation robots. It is equipped with an innovative transmission technology, which provides both high gear ratio and fine reversibility.

In order to evaluate the device and its therapeutic efficacy, we compared several series of pointing movements in healthy subjects wearing and not wearing the orthotic device. In this way, we could assess any disturbing effect on normal movements. Results show that the main movement characteristics (direction, duration, bell shape profile) are preserved.

### I. INTRODUCTION

Physical rehabilitation is not confined to aging-related health problems, but also to stroke or spinal-cord impairments. Medical rehabilitation usually comprises of physical therapy (PT), occupational therapy (OT), and counseling for emotional support. For PT and OT, intensive manual medical attention from therapists is required because effective treatment is based on intensive physical exercise and positioning practice ([1][2],[3]) to assist functional recovery [4].

In the perspective of economics of neurological

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rehabilitation, and its limited treatment options in duration, sophisticated rehabilitation robotic systems can only be of benefit to the medical society and the patients: it can provide effective means of treatment with high functionality, personalization, repeatability, and force scalability.

Amid the growing medical robot industries, there have been quite a few product and research developments in robots specific to upper-limb rehabilitation (see [5]), following the pioneer MIT-Manus [6]. This system has a 2 DoF manipulator that exerts force on the patient's hand through a handle. It thus can provide assistance only at the end-point level, failing to address the crucial problem of assisting the internal motion of the redundant human arm.

This is why an upper-limb orthoses, that patients wear on the whole arm to practice therapeutic exercises, have been more recently investigated. Our work fits in this research area. The technical challenge lies in mechanically enabling total degrees of freedom in the arm while respecting its biomechanics (speed, torque, center of rotation, workspace, etc.), an adequate control bandwidth and algorithm for a transparent human robot interaction, an inherent safety (compliant joints and applied joint torque monitoring), a comfortable physical interface with the patient are just few design criteria for developing a robotic orthosis for comprehensive therapy.

Kiguchi and Fukuda's 3 DoF exoskeleton [4] is developed to assist physical therapy and has safe compliant joints as it is driven by cables from DC motor connections. However, it has a low control frequency due to the naturally unstable EMG signal and a limited range motion designed for minimal task executions just under shoulder height. For a wider range of motion, Haptic arm exoskeleton, MAHI ([7],[8]) has a unique parallel link structure for eliminating singularities and maximizing its workspace which approximately matches that of the human (so does RUPERT, [9]). However, with a price of having either restrictive encasing ([7],[8]) or limited DoF around the shoulder ([7], [8],[9]) reducing its applicability in total upper limb rehabilitation. L-EXOS [10] has 70% of human workspace with sufficient shoulder DoF but with a higher weight and customized parts. With a full 9 DoF [11], 9 DoF passive skeleton device replicates comprehensive DoF of human body and range of motion with its light weight, however, this passive architecture is unsuitable for robot assisted physiotherapy. A portable exoskeleton from KIST [12] has a full 7 DoF for realizing human arm movements. It was designed to idealize human-robot interaction and consequent motion teaching rather than therapeutic usage; therefore, its applicability in rehabilitation usage for guiding patient arms is questionable regarding its actuation

capabilities.

ARMin I and II [13],[14], WREX [15] and CADEN-7 [16] device supports a human arm by having adaptable DoF and range of motion, torque; but their large volume is only suitable for spacious clinical areas.

This paper presents a new design of a portable and reversible cable transmission orthosis, ABLE, that was designed to have a maximum therapeutic effectiveness. This translates into a mechanical design with a minimum backlash and friction actuator, together with a low level control algorithm for a fluid and transparent human robot interaction, all while being safe and comfortable for medical practices. The detailed mechanical design, characteristics and kinematics of the orthosis are covered in Section 2. The experimental setup and procedures used to test robot with healthy subjects are illustrated and explained in Section 3. Section 4 reports the results of the experiment that confirms the validity of the device applicability, through preliminary tests that compared the movements of healthy subjects performing pointing tasks with and without wearing the orthosis programmed to be in a transparent mode.

## II. MECHANICAL DESIGN

### A. General orthosis kinematics

The 4 axes exoskeleton developed for physical rehabilitation is named ABLE (see Fig. 1) by the authors of CEA-LIST. It uses an innovative actuation technology using cable force transmission. ([17],[18],[19][20],[21]).



Fig 1. ABLE 4 axis exoskeleton actuated by screw-and-cable actuators

Its kinematics are composed of a shoulder spherical arrangement made with 3 coincident axes and an elbow. The forearm, terminated by a handle, is not actuated. Its kinematics are sketched in Fig. 2, and the Denavit & Hartenberg parameters are shown in Table 1.

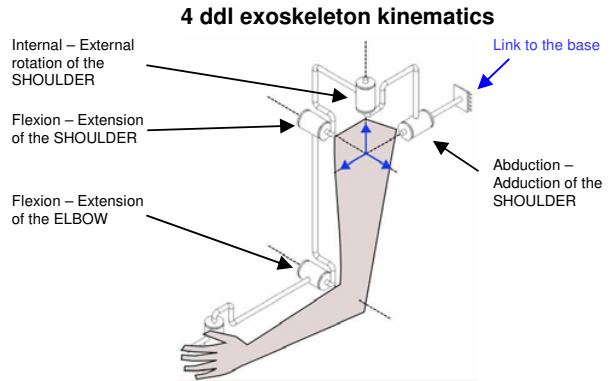


Fig 2: Kinematics of ABLE

| $i$ | $a_i$    | $\alpha_i$ | $\theta_{i+1}$ | $d_{i+1}$ |
|-----|----------|------------|----------------|-----------|
| 0   | $-\pi/2$ | 0          | $\theta_1$     | 0         |
| 1   | $-\pi/2$ | 0          | $\theta_2$     | 0         |
| 2   | $\pi/2$  | 0          | $\theta_3$     | 0         |
| 3   | $-\pi/2$ | 0          | $\theta_4$     | $d_1$     |

Table 1: DH parameters of ABLE

### B. Transmission – Actuators

Most of the technological originality of ABLE comes from its actuation and transmission system, which is based on a CEA-patented Screw-and-Cable System (SCS) [22].

The SCS actuator design principle is as follows (see Fig 3): a hollow screw is locked in rotation - the nut rotating in a bearing - and translates without being guided linearly. The locking device – a simple pair of rollers moving inside a slot – is coupled to the screw by a flexible coupling in order to absorb beating oscillations resulting from the lack of linear guiding. A transmission cable is attached in the middle. Due to the radial backlash between the cable and the bore of the screw, beating oscillations are not counteracted and the misalignment of the cable has virtually no influence on the bending moment of the screw. The result is a regular and a very low friction threshold and the efficiency of the screw is neither affected by any geometrical defaults nor by the eventual deformation of the structure under load.

The overall advantages of the SCS transmission are:

- A high force capacity, thanks to a high overall gear ratio;
- A low friction threshold and high backdrivability;
- An alignment of the motor parallel to cable, which permits highly compact arrangement as compared to transversal motors or beveled gearboxes;
- A low inertia and high stiffness;
- A high tolerance to manufacturing incertitude and to structure flexibility, which allows a wide choice of structural material.

The SCS also benefit from inherent advantages of the cable transmissions, which are shock absorption capabilities, smoothness, high efficiency, versatility (efficient angle transmission, intricate routings through joints).

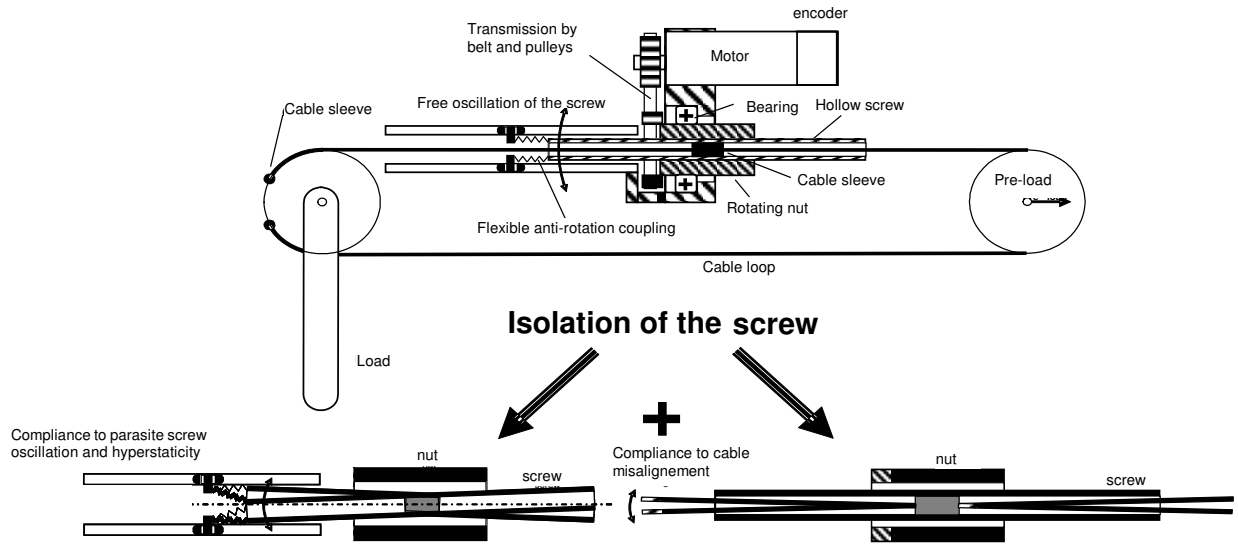


Fig 3. Basic principle of a SCS

An important capability is the tolerance to vibrations of the rotating parts like, the screw, as much as cable misalignments, thanks to a minimized cable fixation area and flexible couplings placed between screw and cable guidance parts (See Fig. 3). Details on the designs and features of the SCS can be found in [19], [21].

In the ABLE exoskeleton, the SCS are partially embedded in limb very much alike electrical muscles, as illustrated in Fig. 4.

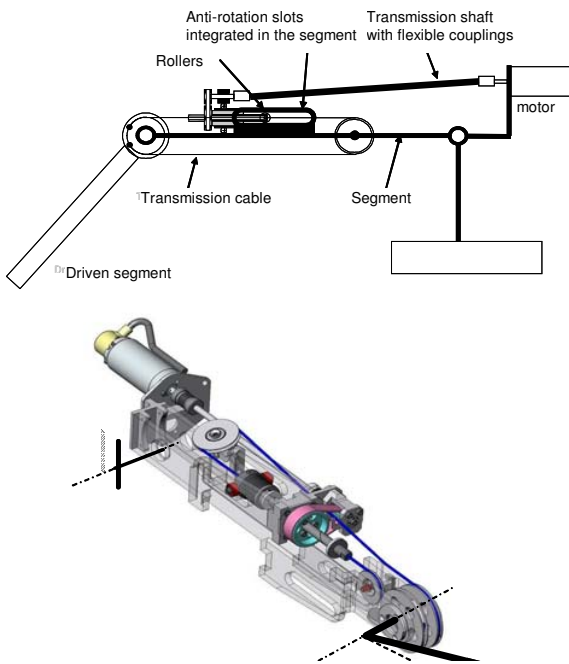


Fig 4. Scheme of an embedded SCS

The integration of the cable loop inside the limb shortens the cable and increases the transmission stiffness, whereas

the location of the motors close to the joint axis drastically decreases the inertial effect of embedded motor masses, resulting in a satisfactory tradeoff.

Each of the back and arm modules integrates two SCS. The overall mass/volume of the mechanics is then spread along the structure allowing to closely follow the human morphology and achieve a better balance.

Figure 5 shows ABLE's transmission kinematics. The back module drives the two first axis of the shoulder (Joint 1 and 2). The arm module drives two transversal axis (Joint 3 and 4). Joint 3 is the third axis of the shoulder making it an equivalent of a spherical articulation, while Joint 4 is the elbow axis.

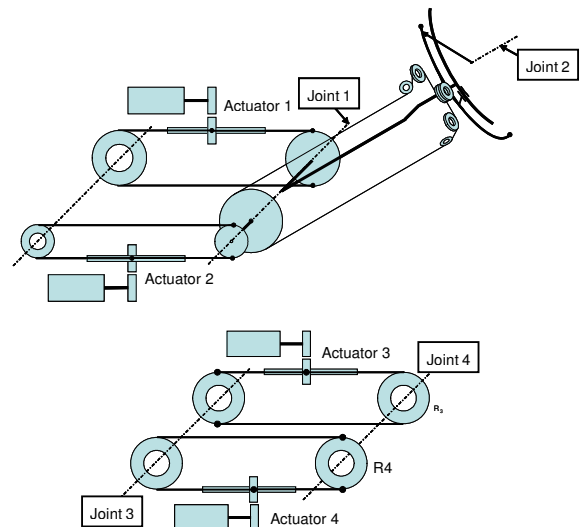


Fig 5. Back module transmission and shoulder (top) – Arm module transmission (bottom)

The shoulder design is kept simple and discrete. It is made of a part that articulates on the back (Joint 1) and also

supports a circular guide which defines a second virtual axis perpendicular to the first (Joint 2). Their intersection defines the virtual center of the exoskeleton spherical.

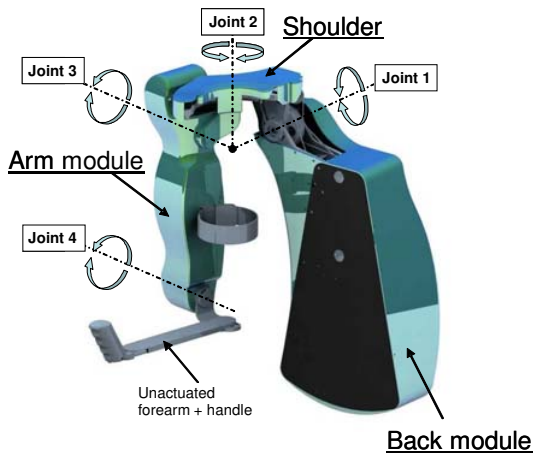


Fig 6. General view of ABLE

It is important to note that the back module may receive the motorization of the second exoskeleton without increasing in volume.

The arm mass with the motors is 2,3 kg. The table 2 below summarizes the other basic mechanical specifications of ABLE.

| JOINT                              | Axis 1                     | Axis 2                       | Axis 3              | Axis 4              |
|------------------------------------|----------------------------|------------------------------|---------------------|---------------------|
|                                    | Abduction / Adduction      | Rotation Internal / External | Flexion / Extension | Flexion / Extension |
|                                    | SHOULDER                   |                              |                     | ELBOW               |
| Amplitude                          | 110 °                      |                              |                     |                     |
| Motors                             | DC Faulhaber type          |                              |                     |                     |
| Transmission                       | Ball-screw and cable (SCS) |                              |                     |                     |
| Speed (cartesian)                  | >1m/s                      |                              |                     |                     |
| Joint torque (continuous)          | 18 Nm                      | 18 Nm                        | 13 Nm               | 13 Nm               |
| Continuous effort in hand          | 50 N                       | 50 N                         | 40 N                | 40 N                |
| No-load friction in hand (approx.) | 3 N                        |                              |                     | 2 N                 |

Table 2: ABLE basic specifications

## II. EVALUATION OF A TRANSPARENT CONTROLLER FOR MAN-ORTHESES INTERACTION

For intricate and specific human robot interaction requirements imposed by medical applications, the hardware characteristics of ABLE serve as an excellent platform for the physical rehabilitation therapies. Its low joint stiffness and naturally compliant joints ensure the safety while using the robot for patients with physical disability. As a part of the BRAHMA project, the authors have built the hardware, applied control schemes with a high transparency, and had human subjects to try the device. In this section, the focus of the experiment, the control architecture for running the tests, and methods and procedures for evaluating the robot performance and its efficacy on volunteer subjects are described.

### A. Aim

The overall aim of the BRAHMA project is to design and control a robotic orthosis suitable for rehabilitation of the hemiparetic upper limb. Prior to beginning testing on patients, it was imperative to assess the influence of the robot on arm movement in healthy subjects first.

The aim of the experiment was twofold. The first aim was to evaluate the transparency of the robotic-orthosis. If it is totally transparent, kinematic parameters during pointing movements should not be different from kinematic parameters during the same pointing movements without the orthosis. The parameters evaluated to determine this were peak hand tangential velocity, the number of peaks in the hand velocity curve (indication of smoothness [22] ) and curvature of hand path (namely the ratio of the total length of the trajectory on the 3D distance between the beginning and end of the movement). The second aim was to assess if the subject's arm moved within the orthosis during movements to different parts of the workspace. To ascertain this information, the difference in distance between two adjacent markers near the elbow (one on the orthosis, the other on the subject) was calculated at the start and end positions for each target.

### B. Controller

The torque of the motor is in general, a combination of gravity compensation torque (computed) and a reaction torque computed from an position error signal, the difference between the awaited position and the measured position (PID controller). Therefore a position error denotes an output force exerted either by the operator or by a contact with an object. In quasi-static situations, the proportionality between the position error and the exerted force is directly dependant upon the amount of friction in the transmission as shown on Fig 7. In absence of contact/reaction force the system can be moved under a residual effort given by the distance between the red/blue point and the black point along the y axis. This principle allows us to get a reasonably backdrivable system while using only joint position sensors. More explanations about the controller can be found in [17].

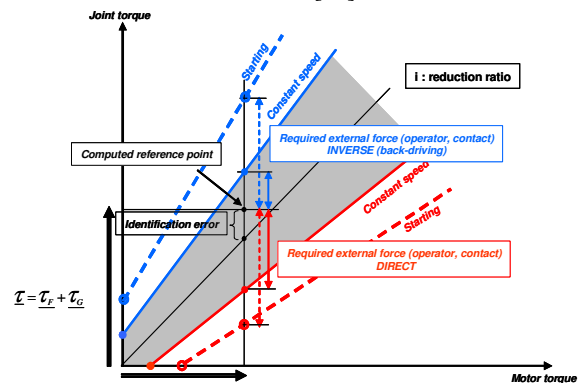


Fig 7. Input-Output force transmission diagram

The robot controller architecture for the experiments is based on a PC104 board with two endowed 3 channel axis controller. It runs at 1kHz the control law thanks to a real time operating system (RTlinux).

As the orthotic device is only fitted with optical encoders, we do not have access to an acceleration signal. For those preliminary experiments mainly focused on the mechanical evaluations, only simple compensations were used to achieve transparency. No trajectory were sent to the controller and transparency was achieved thanks to a gravity compensation for all axis and also a compensation for the residual dynamic dry friction compensation for two axis of the shoulder (the ones for shoudler rotation and abd/adduction which have the greatest reduction ratio see Fig. 5). This residual friction compensation has been developed in order to blend the friction phenomenons on all axis, and so on not to lead subject to do non-natural moves because of feelings differences on every joints.

### C. Methods

Motion tracking was carried out using 2 Codamotion units. The Codamotion system consists of active LED markers each with an individual emitting frequency. Their 3D displacement is captured by wide-angle sensors. 5 infra-red-LED markers were positioned on the orthosis and seven on the subject's upper limb (Fig 8.a). Note that the usual anatomical points could not be used because many were hidden by the orthosis. Biometric data were measured for each subject for further dynamical analysis. Acquisition frequency was 100Hz.

Nine targets were positioned such in a way as to evaluate movements in different parts of the subject-robot workspace. Target position was determined for each subject by placing the targets so that the shoulder was flexed at 80° and the elbow flexed at 15° for the high targets.

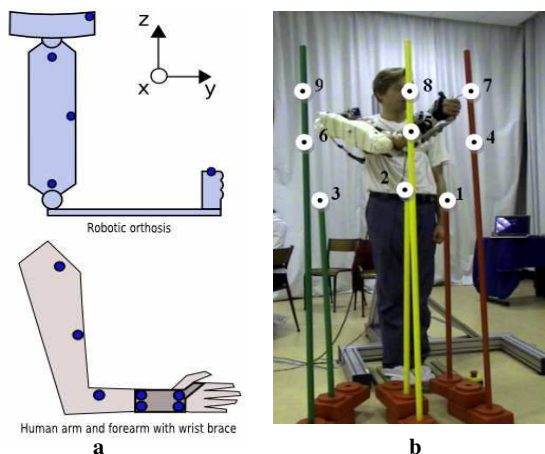


Figure 8. a. Position of Codamotion markers on orthosis and subject ; b. Subject pointing to target 7 wearing orthosis. Positions of all targets shown.

with the subject's shoulder and 30° to the left and right (Fig 8b).

The height of the orthosis on its column was adjusted for each subject so that the humeral head was aligned with the axis of shoulder rotation of the orthosis. Subjects wore a wrist brace since wrist movement was not possible while wearing the orthosis, we also wished to prevent wrist movements in the free condition. The trunk was also fixed

### D. Subjects

At present the segment lengths of the orthosis are fixed and is designed for a tall person. As such, only tall males were recruited. 5 healthy subjects of height 1.82m-1.98m aged between 25 and 30 years, naïve to the project agreed to participate.

### E. Task

Subjects were asked to make three consecutive movements to each target (the target order was pseudo-randomised), at natural speed when wearing and not wearing the orthosis. Recordings were also made of a single out and back movement with the robot at maximum subject speed ("rapid with orthosis" curves) to evaluate the impact of inertia phenomenons on human arm trajectory. All movements with and without the orthosis were carried out with the subject in the same initial position.

## III. RESULTS AND DISCUSSION

As expected, the peak movement velocity varied according to the target distance and position (Fig 9). The average velocity of self-paced movements was  $1.3 \pm 0.5$  m/s in the free condition and significantly decreased to  $0.9 \pm 0.3$  m/s while wearing the orthosis ( $p < 0.0001$ ). Fast movements carried out with the orthosis ( $1.6 \pm 0.3$  m/s) were only slightly faster than self-paced free movements. This indicates that the robotic-orthosis restricts movement velocity.

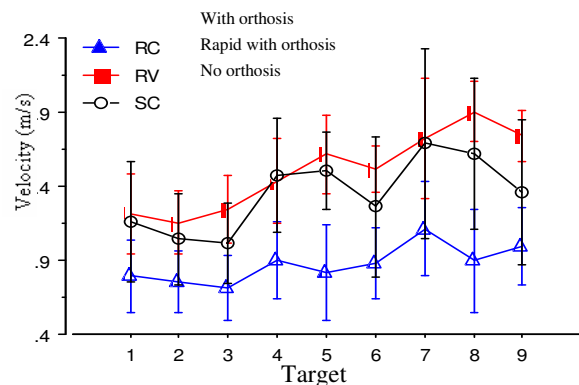


Figure 9. Average peak velocity (and SD) to each target according to condition.

Normal voluntary 3D reaching movements are characterized by a bell shaped velocity curve with a single peak [24]. The velocity curves for movements while wearing the orthosis had significantly more peaks suggesting a loss of smoothness ( $1.7\pm 0.8$  peaks without orthosis,  $3.5\pm 1.9$  with orthosis ( $p<0.0001$ )). The fast movements while wearing the orthosis; however, had less peaks than the self-paced movements with the orthosis ( $2.3\pm 1.0$ ).

Natural pointing movement trajectories are often slightly curved. This is indicated by a curvature ratio of the tangential displacement which is greater than 1 in the free condition ( $1.07\pm 0.05$ ). This ratio varied with the target and its average increased significantly while wearing the orthosis ( $1.13\pm 0.1$ ); however, the effect of wearing the orthosis varied with the position of the target (Fig 10).

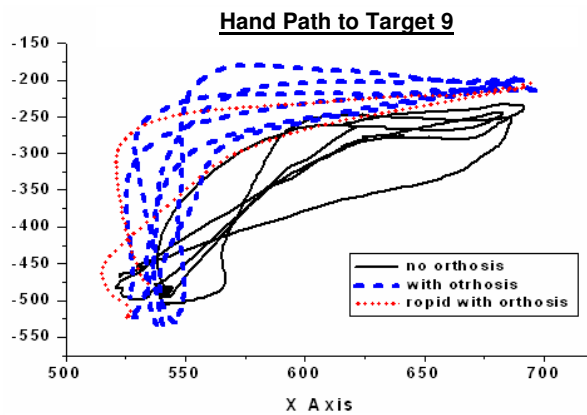


Figure 10. Hand paths viewed from above to one target (the target 9 which is high and external). The orthosis modifies the trajectory dependant on direction.

For the same movement toward the target, the velocity curves show some segmentation compared to the free-state's ideal curve, which would be in a smooth bell shape (Fig 11). The curvature of the movement to external-high target was significantly higher with the orthosis while it was decreased for a forward-middle target. This demonstrates that the orthosis imposed some mechanical constraints on the movement.

However, the effect of increasing movement velocity (average curve ratio  $1.12\pm 0.08$ ) was not clear, suggesting that the deformation of the trajectory was not only due to inertial constraints.

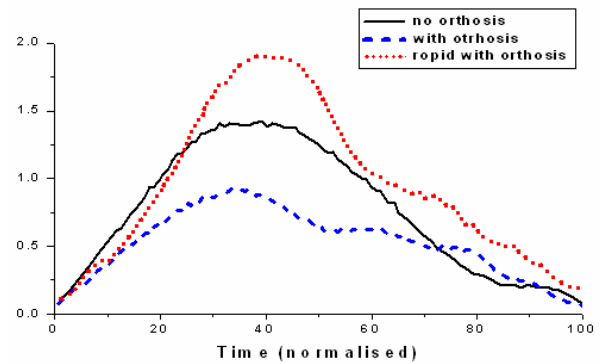


Figure 11. Velocity curves for movements to target 9 for one subject in the three conditions.

Movement of the subjects' arms relative to the orthosis was ascertained by the difference in tangential distance of the marker on the subject's lower humerus to the adjacent marker on the orthosis. There was an average movement of  $3.1\text{cm} \pm 1.9$ . This movement was generally greater for higher targets.

#### IV. CONCLUSION

The developed orthosis, ABLE, received positive feedback from the participating subjects who were able to make a wide range of movements in 3D. However, it induced some clear alteration in self-paced motion trajectories: meaning that the transparency of the ABLE during the general slowing and modification of trajectory is still limited. Further analysis of exact physical effects in joint and actuator rotations are needed to determine the mechanism of these effects: role of inertial and viscous constraints, effect on the synchronisation of the robotic and human joints rotations.

One of the main application of an exoskeleton is for physical rehabilitation where it can control the movement of each segment. Therefore, the movement of the robot, ABLE, can produce movements closer to that of the human. The ABLE will be used to rehabilitate normal inter-joint synergies that are impaired in hemiparetic stroke patients and discourage pathological synergies[25],[26].

Our future work is now focused on two points. One is to improve control transparency (more transparent control scheme can be used for patients who has made a large recovery in the movements in order not to badly impact patient moves which do not need robot assistance). We are currently working on improving the transparency by predictions from the movement invariants. And another point is to have a larger patient test consensus (especially the test cases when the ABLE is active and drives the arm of a patient for therapy). It is also essential to have a more comfortable and robust physical interface in between the robot and the user. By keeping the isostaticity in this

interface, we expect to minimize any apparent constraint application on the human arm. For this, the benefits of adding the fifth DoF (the wrist prono-supination) will be evaluated in the following research.

#### ACKNOWLEDGMENT

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