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HAL Id: cea-01135495
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Submitted on 25 Mar 2015

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Ion-neutral friction and accretion-driven turbulence in self-gravitating filaments

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Received 23 April 2013 / Accepted 8 October 2013

ABSTRACT

Recent Herschel observations have confirmed that filaments are ubiquitous in molecular clouds and suggest, that irrespective of the column density, there is a characteristic width of about 0.1 pc whose physical origin remains unclear. We develop an analytical model that can be applied to self-gravitating accreting filaments. It is based on the one hand on the virial equilibrium of the central part of the filament and on the other hand on the energy balance between the turbulence driven by accretion onto the filament and dissipation. We consider two dissipation mechanisms, the turbulent cascade and the ion-neutral friction. Our model predicts that the width of the inner part of the filament is almost independent of the column density and leads to values comparable to what is inferred observationally if dissipation is due to ion-neutral friction. On the contrary, turbulent dissipation leads to a structure that is bigger and depends significantly on the column density. Our model provides a reasonable physical explanation which could explain the observed filament width when they are self-gravitating. It predicts the correct order or magnitude though hampered by some uncertainties.

Key words. turbulence – stars: formation – ISM: structure – magnetic fields

1. Introduction

With the recent observations performed with Herschel (e.g. André et al. 2010; Molinari et al. 2010), it has become clearer that filaments are ubiquitous in molecular clouds and that they likely play a central role in star formation. While the exact influence filaments may have on the star formation process remains to be clarified, it is important to understand the properties of these filaments since they are a direct consequence of the physics at play within molecular clouds. In this respect, a particularly intriguing observational result was found by Arzoumanian et al. (2013). The plan of the paper is as follows. In Sect. 2, we present the various assumptions and physical processes used in our simple model. Section 3 describes the results and Sect. 4 concludes the paper.

In this paper, we explore the idea that the typical width of a self-gravitating filament is due to the combination of accretion-driven turbulence onto the filament, as suggested by the recent velocity dispersion measurements of Arzoumanian et al. (2013), and to the dissipation of this turbulence by ion-neutral friction which does have a characteristic scale. We stress that although ambipolar diffusion is considered here, the underlying idea is totally different from the classical magnetically regulated star formation (e.g. Shu et al. 1987) in which the magnetic field is envisaged as the dominant support and ambipolar diffusion as the process through which the support can be circumvented. The plan of the paper is as follows. In Sect. 2, we present the various assumptions and physical processes used in our simple model. Section 3 describes the results and Sect. 4 concludes the paper.

2. Model and assumptions

2.1. Characteristics of the filament

Herschel observations (e.g. Palmeirim et al. 2013) suggest that the typical average structure of self-gravitating filaments is constituted by i) a central cylinder of nearly uniform density $\rho_f$ and radius $r_f$; and ii) an envelope whose density profile is $\rho \propto r^{-2}$. This radial structure is reminiscent of many self-gravitating objects such as Bonnor-Ebert spheres. More precisely, filaments that are collapsing in a self-similar manner are expected to present an envelope with a profile $\rho \propto r^{-2/(2-\gamma)}$ where $\gamma$ is the adiabatic index.
of the gas (Kawachi & Hanawa 1998). As it is likely that self-gravitating filaments are collapsing in a way not too different from, although not identical to, a self-similar collapse, assuming an $r^{-2}$ profile is thus a well-motivated assumption, both from observations and theory. One important difference with such self-similar solutions, however, is that the central density plateau does not seem to shrinking with time.

If $L$ is the length of the filament, the mass of the central part is obviously $M_1 = \pi n_0 L^2 = m_1 L$, where $M_1$ is the mass and $m_1$ the mass per unit length. The total mass of the central part plus the surrounding envelope is

$$M_{\text{ext}} = M_1[1 + 2\ln (r_{\text{ext}} / r_1)] \equiv M_1 \mu (r_{\text{ext}} / r_1),$$

(1)

where $\mu(x) = 1 + 2\ln(x)$. It has been assumed that the density outside the filament is $\propto 1/r^2$ and that the filament stops at some radius $r_{\text{ext}}$. Below we assume $r_{\text{ext}} \approx L/2$.

### 2.2. Gravitational potential within the filament

The gravitational potential, in the radial direction is obtained by the Gauss’s theorem

$$r < r_1, \quad \phi(r) = \pi G \rho_1 r^2 = G m_1,$$

(2)

$$r > r_1, \quad \phi(r) = G m_1 \left(1 + 2 \log (r/r_1) + 2 [\log (r/r_1)]^2\right),$$

$$\equiv G m_1 (1 + \mathcal{G}(r/r_1)),$$

where $\mathcal{G}(x) = 2 \ln(x) + 2 [\ln(x)]^2$.

### 2.3. Magnetic field

As the ion-neutral friction dissipation depends on the magnetic field, it is necessary to know its dependence.

We proceed in two steps. First, we discuss the expected value of the magnetic field in the parent clump $B_c$. Second, we infer the value of the magnetic field in the filament $B_f$ from the value of $B_c$.

#### 2.3.1. Magnetic field in the parent clump

The magnetic field in the clump is assumed to be proportional to the square root of the density $B_c = B_0 \sqrt{\rho_c / \rho_0}$ as has been observed (e.g. Crutcher 1999). Typical values are $B_0 \approx 25 \mu G$ and $n_0 \approx 10^3 \text{ cm}^{-3}$, where $n_0 = \rho_0 / \mu_p$. In the following we will use the $B_0 = B_0 / \sqrt{4\pi \rho_0} \approx 1 \text{ km s}^{-1}$ as a fiducial value.

We note that the magnetic field dependence is still under debate and that there are alternative choices. First, as suggested by Basu (2000), the magnetic field could scale as $\sigma \sqrt{\rho}$, where $\sigma$ is the velocity dispersion, rather than just as $\sqrt{\rho}$. Second, Crutcher et al. (2010) now favor $B \propto \rho^{1/3}$. These relations do not represent large variations and would therefore not affect our results very significantly.

#### 2.3.2. Magnetic field in the filament

To link the magnetic field in the filament to the magnetic field in the parent clump, we proceed as follows. First we assume that the magnetic field is perpendicular to the filament. This configuration is well supported by observations in massive filaments such as Taurus (Heyer et al. 2008; Palmeirim et al. 2013) or DR21 (e.g. Kirby 2009), and is also natural on physical grounds as the gas is expected to accumulate preferentially along the field lines. This implies that at least a fraction of the gas accreted by the filament, is not impeded by the magnetic Lorentz force. There may also be gas accreted perpendicularly to the field lines, which is therefore probably slowed down by magnetic pressure. However, if the field is strong, then most of the material is presumably channeled along the field lines, while if the field is weak it also has a weak influence.

Second, we assume flux freezing which at these scales is a reasonable assumption. This implies that the magnetic field in the filament is simply the magnetic field in the clump compressed along the direction perpendicular to the field and the filament axis. Thus $B_f = B_c \times \eta L / r_f$ since the matter that is inside the radius $r_f$ comes from a distance comparable to the clump’s size, $\eta L$, where $\eta$ typically varies with time between 0 and 1/2. A similar reasoning can be applied to get a relation between $\rho_c$ and $\rho_f$ since $M_1 \propto \rho_f L 
 \propto \rho_f^2 L^3$. We thus obtain $\rho_f = \rho_c (\eta L / r_f)^2$. Combining the expression for $B_c$ obtained above with the last expression, we get $B_f = B_0 \sqrt{\rho_c}$ that is to say, the magnetic field in the filament is also expected to be nearly proportional to $\sqrt{\rho_c}$ implying that the Alfvén velocity should remain nearly constant.

This relation is valid as long as flux freezing can be assumed. While this is a reasonable assumption in the collapsing envelope, which is not magnetically supported, it is not the case in the central part, which is presumably close to equilibrium. The typical ambipolar diffusion timescale is given by Eq. (13) below. For densities on the order of $10^{-7} \text{ cm}^{-3}$, the field is diffused in about 0.1–1 Myr, which is shorter than or comparable to the accretion time of the filaments. Moreover, as emphasized by Santos-Lima et al. (2012) and Joos et al. (2013), turbulence also tends to diffuse out the field. However since self-gravitating filaments are probably accreting, the magnetic flux cannot leak out far away since it is confined by the infalling gas. Therefore, while the mean magnetic intensity within the central part of these filaments is probably on the order of $B_t = B_0 \sqrt{\rho_c}$, it is likely that the magnetic field gradient is greatly reduced with respect to the ideal MHD case.

### 2.4. Virial equilibrium

The virial theorem is applied to the filament inner part of radius $r_f$. The expression for a filament is (e.g. Fiege & Pudritz 2000)

$$2 \int P \, dV + 2 E_{\text{kin}}^{\text{fil}} = W_{\text{grav}} + 2 P_{\text{ext}} V,$$

(3)

where $W_{\text{grav}}$ is the gravitational term, $P$ and $P_{\text{ext}}$ are the internal and external pressure, and $V$ the volume; $E_{\text{kin}}^{\text{fil}} = 0.5 M_f (2 \sigma_{1D}^2)$ is the kinetic energy in the direction perpendicular to the filament axis and $\sigma_{1D}$ is the non-thermal one-dimensional velocity dispersion. This expression is, however, not strictly valid since our model filament is accreting. Additional terms should be taken into account (see Goldbaum et al. 2011 and Hennebelle 2012) which corresponds to the surface terms that do not cancel out as it is usually the case. When the surface terms are taken into account, the virial expression becomes

$$\frac{1}{2} M_f \frac{d \sigma^2}{dM} + 2 \int P \, dV + 2 E_{\text{kin}}^{\text{fil}} = W_{\text{grav}} + 2 (P_{\text{ext}} + P_{\text{ran}}) V.$$

(4)

At this stage we do not consider the influence that the magnetic field may have on the equilibrium because it is not expected to change our conclusions qualitatively. In particular, as discussed in the previous section, the magnetic gradient within the central
part of the filament is probably smoothed because of ambipolar diffusion. Another complication arises because the anisotropy introduced by the magnetic field is perpendicular to the filament axis, which would require a bi-dimensional analysis.

Using the different expressions obtained above we get
\[ \frac{1}{2} \frac{m_i^2}{m_f} \frac{d\sigma_f^2}{dt} + 2c_i^2 + 2\sigma_f^2 = Gm_f + 2P_{\text{ram}} \rho_f, \]
where \( P_{\text{ram}} \) is the ram pressure exerted by the incoming flow and where the pressure of the external medium has not been taken into account. The ram pressure will be estimated below. For the sake of simplicity, we will also use the simplified form of the virial equilibrium
\[ 2\sigma_f^2 \approx Gm_f. \]

2.5. Mechanical energy balance

The mechanical energy balance within the cylinder of radius \( r_f \) leads to
\[ \frac{\sigma_f^2(r_f^2)}{2r_{\text{diss}}} \approx \epsilon_{\text{eff}} M (\phi(r_{\text{ext}}) - \phi(r_f)). \]

Obviously, the left hand-side is the dissipation which can be due either to the turbulence cascade or to the friction between ions and neutrals as described below. We note that it is assumed that the turbulence is isotropic which is why \( \sigma_f^2 \) is used. The right-hand side describes the source of turbulence which is due to the accretion onto the central part of the filament (Klessen & Hennebelle 2010). The efficiency \( \epsilon_{\text{eff}} \) is not well known. Klessen & Hennebelle (2010) proposed that it can be related to the density contrast between the density of the incoming flow and the density of the actual gas in which energy is injected. In the present case, the accretion shock may not be clearly defined because of the turbulent nature of the flow. In any case, the present calculation remains largely indicative at this stage. Below, the value \( \epsilon_{\text{eff}} = 0.5 \) is used because it leads to good agreement with the data. We stress that since our model remains indicative, \( \epsilon_{\text{eff}} \) could also take into account various other uncertainties. For the sake of simplicity, we have also ignored terms associated to the volume variation and the external pressure (e.g. Goldbaum et al. 2011) as they do not modify the results substantially, but make the mechanical energy balance much more complex.

2.6. Accretion rate

The accretion rate remains uncertain since it is difficult to infer observationally (see however Palmeirim et al. 2013 for an estimate in the case of the Taurus B211/3 filament). Here, we consider two different possibilities. This will allow us to test the robustness of our conclusion.

2.6.1. Gravitational accretion rate

To estimate the accretion rate, we assume that it can be computed from the density within the parent clump and the infall velocity. Assuming that the parent clump has a cylindrical radius of about \( L/2 \) and a length equal to \( L \), we get
\[ M = \pi L^2 \rho_c V_{\text{inf}}. \]

The infall velocity is due to the gravitational field of the filament which is given by Eq. (2). We assume that the material which enters the clump at radius \( r = L/2 \) has no initial velocity and we estimate the infall velocity at \( r = L/4 \) leading for \( V_{\text{inf}} \)
\[ V_{\text{inf}} \approx \sqrt{2Gm_f} \left( \frac{L}{2r_i} - \frac{L}{4r_i} \right)^{1/2}. \]

We note that this is again a rough estimate, but since the gravitational potential varies logarithmically with \( r \), this estimate does not depend severely on these assumptions.

The density within the clump is also needed to get the accretion rate and we assume that \( \rho_c = \rho_m \rho_f \) follows the Larson relations (Larson 1981; Falgarone et al. 2009; Hennebelle & Falgarone 2012), \( \rho_f \) being the mass per particle
\[ n_f = n_0 \left( \frac{R_c}{1 \text{ pc}} \right)^{-\gamma_1}, \sigma_3D = \sigma_0 \left( \frac{R_c}{1 \text{ pc}} \right)^{\gamma_2}, \]
where \( n_f \) is the clump gas density and \( \sigma_3D \) the internal rms velocity. The exact values of the various coefficients remain somewhat uncertain. Originally, Larson (1981) estimated \( \eta_d = 1.1 \) and \( \eta_d = 0.38 \), but more recent estimates (Falgarone et al. 2009) using larger sets of data suggest that \( \eta_d = 0.7 \) and \( \eta_d = 0.45-0.5 \). For the sake of simplicity, we use \( \eta_d = 1 \) and take \( n_0 = 1000 \text{ cm}^{-3} \).

\[ M = \pi L^2 \rho_v(1 \text{ pc})^{\gamma_v} \sqrt{2Gm_f} \left( \frac{L}{2r_i} - \frac{L}{4r_i} \right)^{1/2}. \]

The typical accretion timescale is simply given by \( \tau_{\text{accret}} = M/J_\text{tot} \). With Eq. (10), it is easy to show that
\[ \tau_{\text{accret}} \propto \sqrt{\rho_v}. \]

2.6.2. Turbulent accretion rate

As it is not clear what controls the accretion rates onto interstellar filaments, we also consider the turbulent accretion rate constructed from the Larson relations described in Hennebelle (2012),
\[ M = M_{\text{tot}} \frac{\tau_e}{2r_\text{c}(\sigma_3D/\sqrt{3})} \approx M_0 \left( \frac{M_{\text{tot}}}{M_0} \right)^{\eta_{\text{acc}}}, \]
where \( \eta_{\text{acc}} \approx 0.7-0.8 \) depending on the exact choice of the parameter \( \eta_d \) and \( \eta_d \) is that retained. We will adopt \( \eta_{\text{acc}} \approx 0.75 \) as a fiducial value. We typically have \( M_0 = 10^{-3} M_\odot \text{ yr}^{-1} \) for \( M_0 = 10^4 M_\odot \).

2.6.3. Ram pressure

The ram pressure which appears in Eq. (5) can be estimated as follows. It is equal to the product of \( V_{\text{inf}}(r_f^2) \) and \( \rho_m = M/(2\pi r_\text{c}L V_{\text{inf}}(r_f)) \), where \( \rho_m \) is the density that is obtained assuming a constant accretion rate. We note that \( \rho_m < \rho_c \), which implies that an accretion shock is connecting the infalling envelope and the central part of the filament. Since the above expression assumes that the flow is isotropic, and since we are assuming the structure of the flow rather than inferring an exact solution, this value remains hampered by large uncertainties and is certainly valid within a factor of a few. We have tested the influence of varying the ram pressure by a factor of a few and found that it has a limited influence on the solution at low density, while it has no influence at high density.

2.7. Dissipation timescales

The dissipation timescale to be used in Eq. (7) is a crucial issue. Here we emphasize two dissipation mechanisms, the turbulent cascade time and the ambipolar diffusion time. Quantitative estimates of these two timescales have been recently estimated by Li et al. (2012) in turbulent two fluid MHD simulations. They found that under typical molecular cloud conditions both contribute, but the second dominates over the first.

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2.7.1. Dissipation by turbulent cascade

First, we consider the standard turbulent cascade timescale, which is the crossing time of the system

\[ \tau_{\text{dissc}} = \frac{2r_t}{\sigma_{ID}} \]  

(12)

The energy cascades to smaller and smaller scales until the size of the eddies reaches the viscous scale.

2.7.2. Dissipation by ion-neutral friction

Second, we investigate the dissipation induced by the ion-neutral friction. Its expression was first inferred by Kulsrud & Pearce (1969, see also Lequeux 2005) and is given by

\[ \tau_{\text{dissemb}} = \frac{2\gamma_{\text{damp}} \rho_i}{v_A^2 (2\pi/\lambda)^2} = \frac{2\nu_i}{v_A^2 (2\pi/\lambda)^2}. \]  

(13)

where \( v_A \) is the Alfven speed, \( \lambda \) is the wavelength assumed to be equal to \( r_t \) and \( \nu_i \) is the ion-neutral coupling coefficient. The reason we choose \( \lambda = r_t \) is that if most of the energy is dissipated at a scale much smaller than \( r_t \), then the relevant time would be the crossing or cascading time that would be necessary for the energy to cascade from \( r_t \). In this case, the timescale would thus be similar to the turbulent cascade timescale discussed above. The coefficient \( \gamma_{\text{damp}} = 3.5 \times 10^{-13} \text{cm}^3 \text{s}^{-1} \) is the damping rate. The ion density, \( \rho_i \), is assumed to be \( \rho_i = C \sqrt{v_{\text{th}}} \) where \( C = 3 \times 10^{-16} \text{cm}^{-3/2} \text{g}^{1/2} \). For wavelengths \( \lambda < \lambda_c = \pi v_A/(\gamma_{\text{damp}} \rho_i) \), the critical wavelength, the Alfven waves do not even propagate except at very small wavelengths when the ions and the neutrals are entirely decoupled. With \( n = 10^4 \text{cm}^{-3} \) and \( v_A \approx 1 \text{ km s}^{-1} \), \( \lambda_c \approx 5 \times 10^{-2} \text{ pc} \).

We note that the expression stated in Eq. (13) is strictly valid only for Alfven waves. The corresponding expression for the compressible modes has been inferred by Ferrière et al. (1988). They are slightly more complex as it entails the angle between the field and the direction of propagation, but the order of magnitude is not different.

3. Results

To infer the radius of the filament as a function of the central density \( \rho_t \) we have to combine Eqs. (2), (6), and (7) together with the accretion rate given by Eq. (10) or Eq. (11). With the gravitational accretion rate (Eq. (10)), we obtain

\[ \rho_t^{1/2} r_t = \frac{4}{3} \sqrt{2} \pi \epsilon_{\text{eff}} \rho_0 (1 \text{pc}) \sqrt{G} G_1 (L/r_t), \]

\[ \frac{\tau_{\text{dis}}}{\tau_{\text{acc}}} = \frac{4 \epsilon_{\text{eff}} M_0 G_2 (L/r_t)}{3 M_0 (L/r_t)^{1-\eta_{\text{acc}}}} \]  

(15)

\[ \eta_{\text{acc}} \]

where \( G_1 (u) = (G(u/2) - G(u/4))^{1/2} G(u/2). \) With the turbulent accretion rate (Eq. (11)), we get the relation

\[ \frac{\tau_{\text{dis}}}{\tau_{\text{acc}}} = \frac{8 \sqrt{2} \epsilon_{\text{eff}} M_0 G_2 (L/r_t)}{3 \pi^{3/2-\eta_{\text{acc}}} \sqrt{G} M_0^{\frac{3/2-\eta_{\text{acc}}}{2}} (L/r_t)^{1-\eta_{\text{acc}}}} \]

3.1. Dynamical equilibrium with turbulent dissipation

Combining Eq. (12) with Eq. (6), we get \( \tau_{\text{dis}} = \frac{3\sqrt{2}}{\sqrt{\rho_0}} \) which in turn together with Eq. (15) leads to the expression

\[ r_t = \rho_t^{-1/4} \left( \frac{8 \sqrt{2} \epsilon_{\text{eff}} M_0 G_2 (L/r_t)}{3 \pi^{3/2-\eta_{\text{acc}}} \sqrt{G} M_0^{\frac{3/2-\eta_{\text{acc}}}{2}} (L/r_t)^{1-\eta_{\text{acc}}}} \right)^{1/2}. \]

(16)

As can be seen for an accretion rate exponent \( \eta_{\text{acc}} \) of the order of 0.75, we find that \( r_t \propto \rho_t^{-1/2} \), which implies a very weak dependence on the filament radius \( r_t \). For a value of \( \eta_{\text{acc}} = 1 \), we have \( r_t \propto \rho_t^{-1/4} \) which is still a shallow dependence as shown in Fig. 1 where the two expressions stated by Eqs. (17) and (18) are displayed (labeled as friction A and B, respectively).

3.2. Dynamical equilibrium with ion-neutral friction

Combining Eqs. (13) and (6), we infer

\[ r_t = \frac{3 \pi^{3/2-\eta_{\text{acc}}} \sqrt{G} M_0^{\frac{3/2-\eta_{\text{acc}}}{2}} (L/r_t)^{1-\eta_{\text{acc}}}}{2 \sqrt{2} \epsilon_{\text{eff}} \gamma_{\text{damp}} C \rho_0 (1 \text{pc})}. \]

(17)

where we see that \( r_t \) does not depend on \( \rho_t \). That is to say, the width of the filament does not change with its column density as suggested from the results of Arzoumanian et al. (2011). To test the robustness of this result, it is worth investigating what the turbulent accretion rate stated by Eq. (11) is predicting. The corresponding expression is

\[ r_t = \rho_t^{-1/4} \left( \frac{8 \sqrt{2} \epsilon_{\text{eff}} M_0 G_2 (L/r_t)}{3 \pi^{3/2-\eta_{\text{acc}}} \sqrt{G} M_0^{\frac{3/2-\eta_{\text{acc}}}{2}} (L/r_t)^{1-\eta_{\text{acc}}}} \right)^{1/2}. \]

(18)

3.3. A more accurate model

Finally, we investigate the solutions where the thermal support and ram pressure are considered as stated in Eq. (5). The

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Fig. 2. Amplitude of the various terms which appear in the virial equilibrium (Eq. (5)). While at high density the filament equilibrium is due to the balance between gravity and velocity dispersion, it is due to the balance between ram and thermal pressure at low density.

corresponding curve is labeled as friction C. Equation (5) is an ordinary differential equation in \( r \), which can be solved using a standard Runge-Kutta method. Since it is necessary to specify a radius and a density to start the integration, we have explored various cases. We found that for a large range of radii \( r_{\text{start}} \approx 0.01-0.1 \) pc at low density, the solutions quickly converge towards the one that is presented here and for which the radius at \( n = 10^3 \) cm\(^{-3} \) is equal to about 0.05 pc.

As can be seen, more variability is introduced, particularly at low density, where we see that the filament radius decreases at low density. In order to better understand the physical meaning of this solution we plot in Fig. 2, the values of the various virial terms as a function of density.

While the equilibrium between gravity and turbulent support at high density is robust and independent of the choice of the boundary condition, \( r_{\text{start}} \), the behaviour at low density is less robust and varies with it.

It is important to stress a few points. First, the ram pressure term which causes most of the variation remains uncertain since our model is not fully self-consistent in the sense that the density and velocity fields, although reasonable, are not proper solutions of the problem. Second, in the low density regime, the filament is not gravitationally accreting and it is likely that the validity of the model is questionable.

3.4. Comparison of the two dissipation timescales

It is enlightening to compare the values of the dissipation timescales as a function of density for the filament radius corresponding to model B. As expected, the turbulent dissipation timescale is much longer than the ion-neutral friction timescale for densities lower than \( 10^6 \) cm\(^{-3} \). It also increases with density while the turbulent timescale decreases with density. This behaviour is the very reason which explains the nearly constant width of the filaments in our model because as can be seen in Fig. 3, the accretion time presents the same dependence.

To summarize, assuming that the relevant timescale for energy dissipation within the central part of the filament is the turbulent crossing time, we find that the width varies much less with the filament density. This is because, \( \tau_{\text{diss,amb}} \propto \rho_i \propto \sqrt{n_f} \propto \tau_{\text{accret}} \). Since the relevant timescale is the shortest one, which corresponds to the smallest value of \( r_i \), one expects ion-neutral friction to be the dominant mechanism for energy dissipation up to densities of a few \( 10^5-10^6 \) cm\(^{-3} \) (see Fig. 1).

3.5. Comparison with observations

Finally, we confront the present models with the Herschel observational result of Arzoumanian et al. (2011). Figure 4 shows filament width as a function of filament column density. As can be seen, the model based on ion-neutral friction and gravitational accretion (friction B and C) work very well. We note that the model based on turbulent dissipation predicts a constant column density and a variable radius.

4. Conclusion

We have presented a simple model to describe the evolution of accreting self-gravitating filaments within molecular clouds. It assumes virial equilibrium between gravity and turbulence and...
mechanical energy balance between accretion which drives turbulence in the filament and the dissipation of this energy. We show that while dissipation based on turbulent cascade fails to reproduce the narrow range of radius inferred from *Herschel* observations, dissipation based on ion-neutral friction leads to a filament width that depends only weakly on the filament density and is very close to the ≃0.1 pc value, although our analytical approach is hampered by significant uncertainties. We conclude that the combination of accretion-driven turbulence and ion-neutral friction is a promising mechanism to explain the structure of self-gravitating filaments and deserves further investigation.

**Acknowledgements.** We thank the anonymous referee for a constructive and helpful report. We thank Doris Arzoumanian and Evangelia Ntormousi for discussions on this topic. P.H. acknowledge the financial support of the Agence National pour la Recherche through the COSMIS project. This research has received funding from the European Research Council under the European Community’s Seventh Framework Programme (FP7/2007–2013 Grant Agreements No. 306483 and No. 291294).

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